

Utilizing the MATLAB CAPE-OPEN Unit Operation to Make Real Hydrocarbon Mixture Membrane Separation Predictions

Thursday, Oct. 28th, 2021

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Georgia Institute of Technology



Georgia Tech College of Engineering

**School of Chemical and
Biomolecular Engineering**

Our Contribution

Present our experience with using AmsterCHEM's MATLAB Unit Operation.

- Specifically, we implemented our novel shooting algorithm for complex hydrocarbon mixture permeation across asymmetric membrane layers¹

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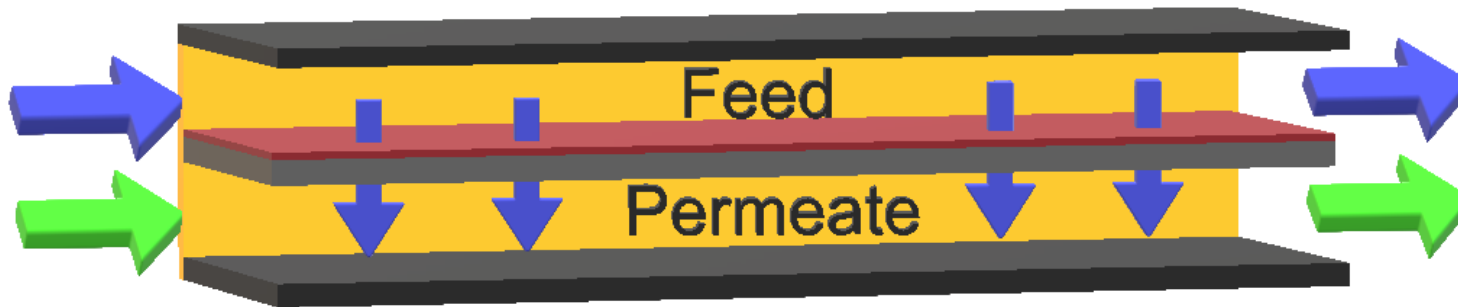
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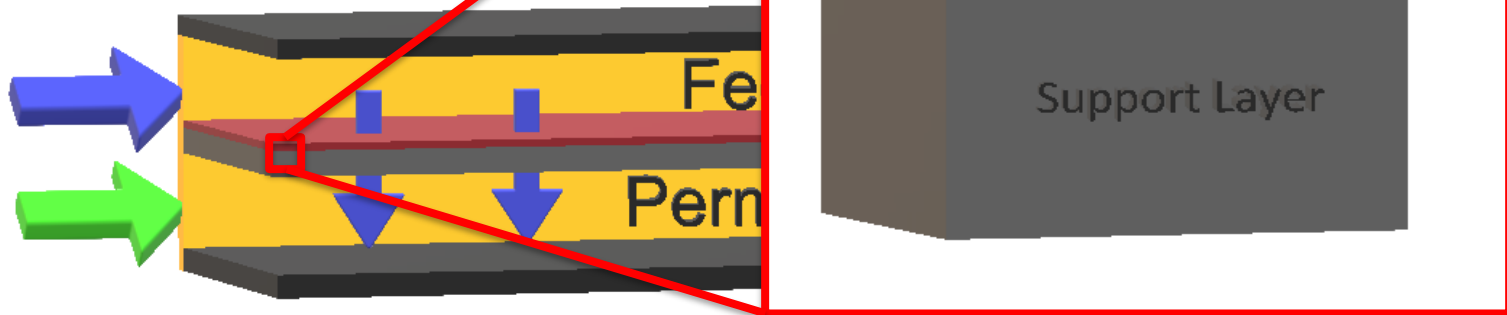
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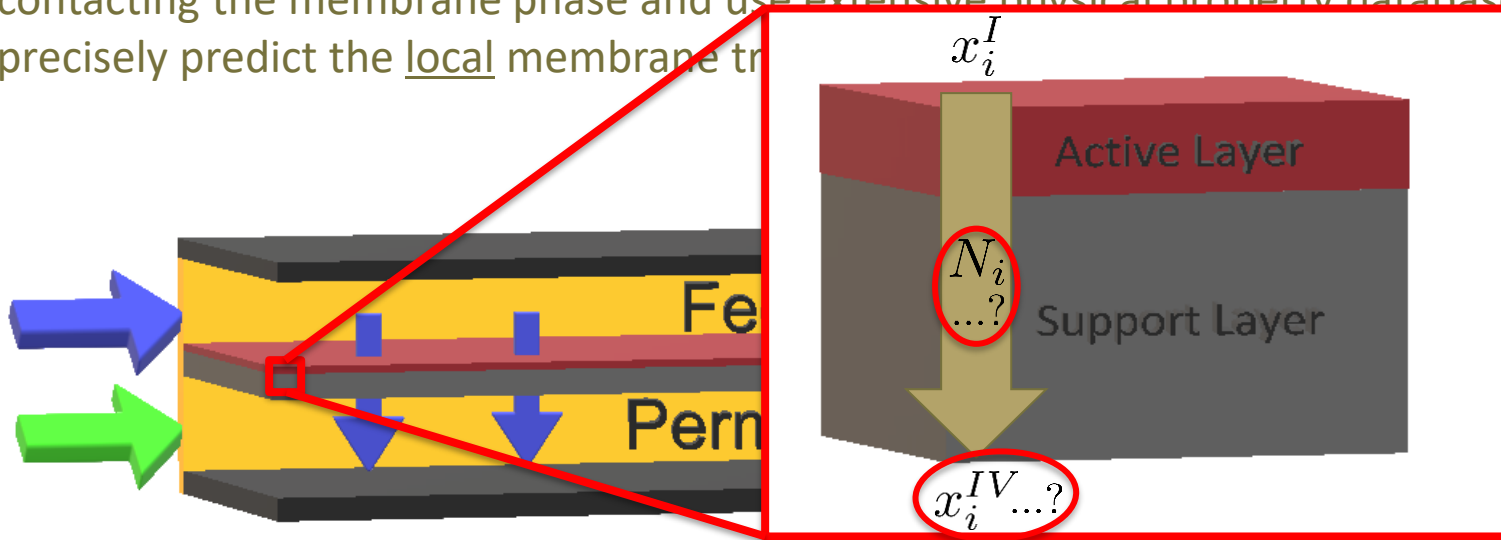
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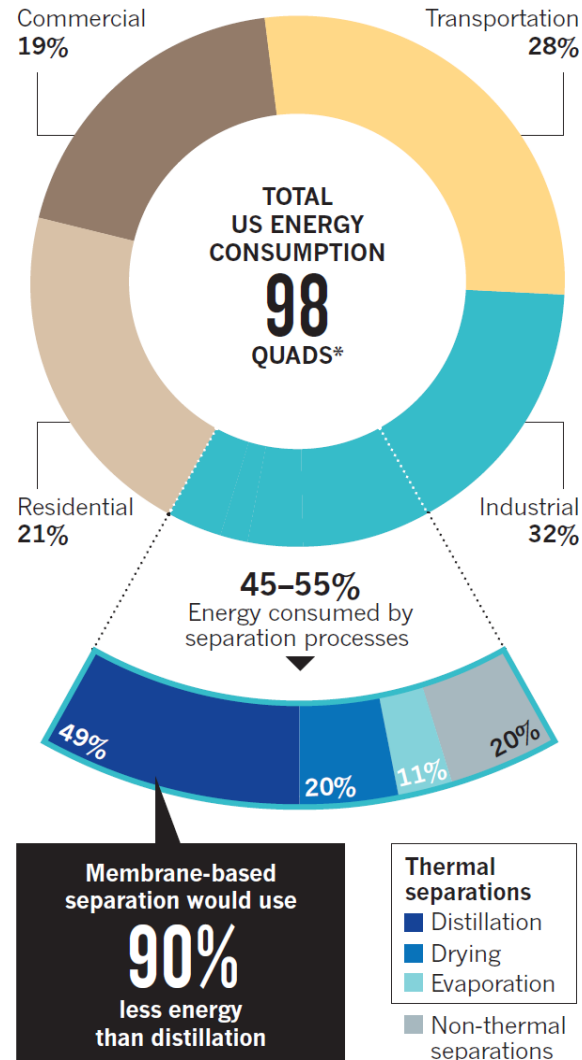
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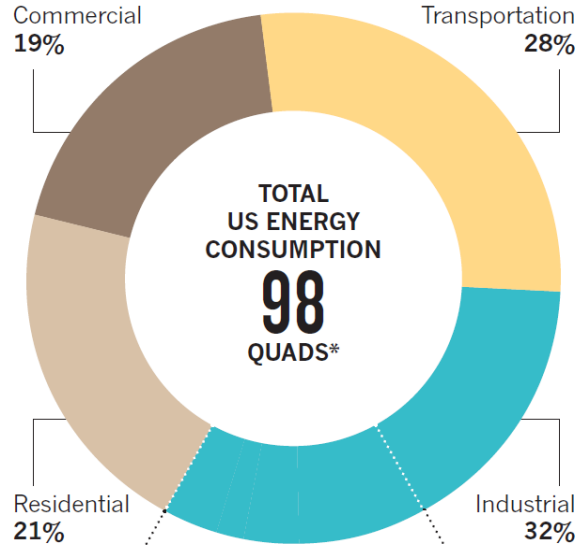
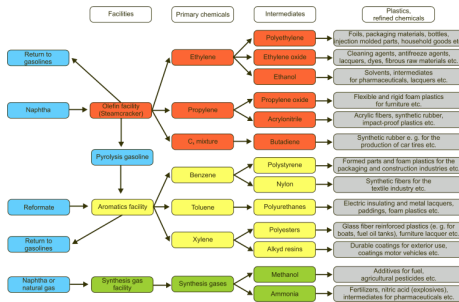


Industrial Membrane Processes

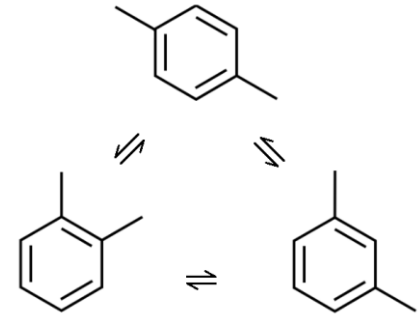


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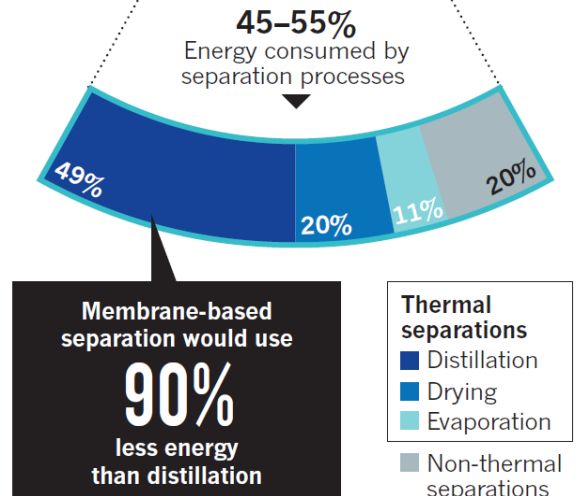
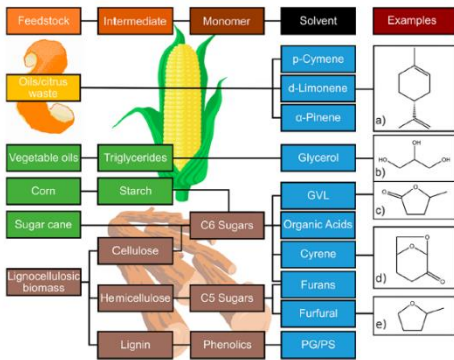
Crude Oil Refining:



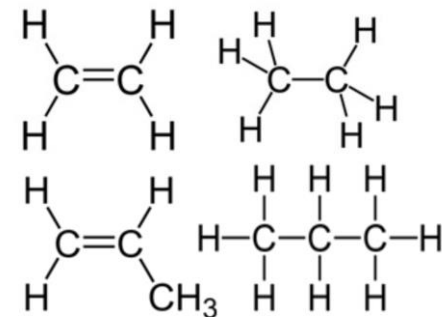
Benzene derivatives:



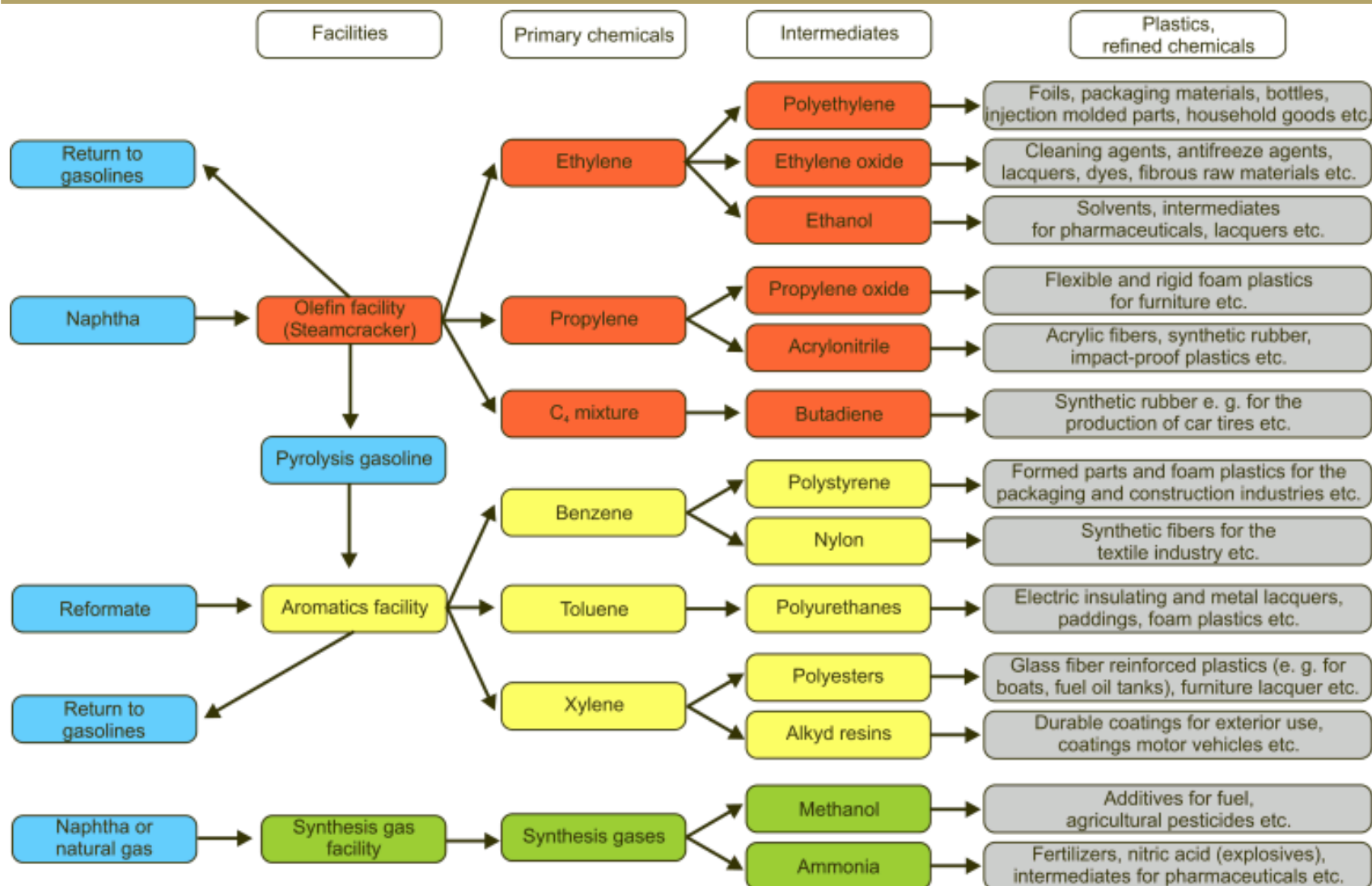
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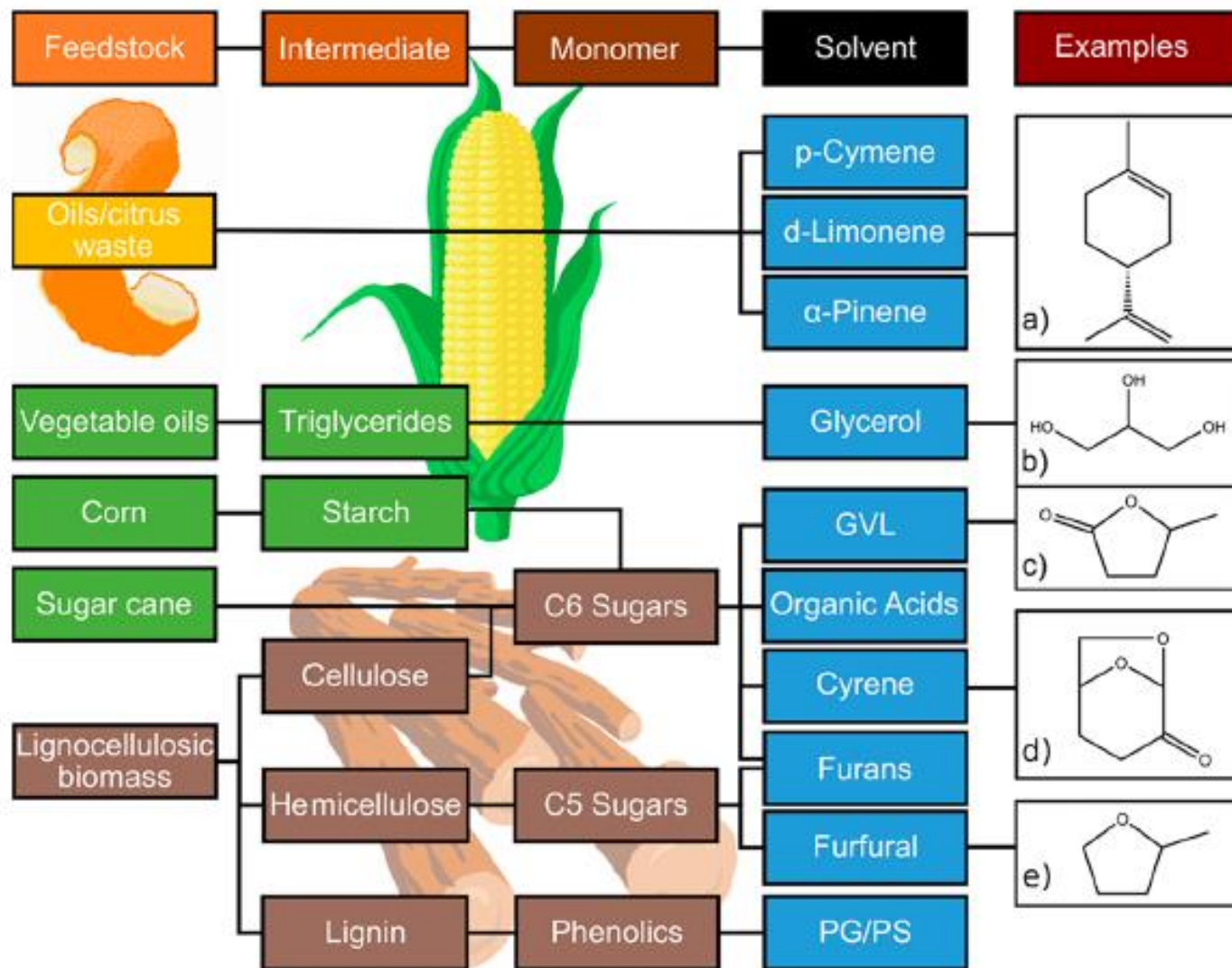
Alkenes from alkanes:



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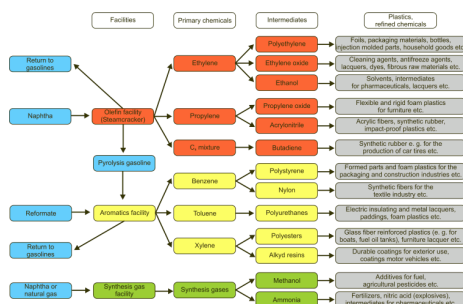


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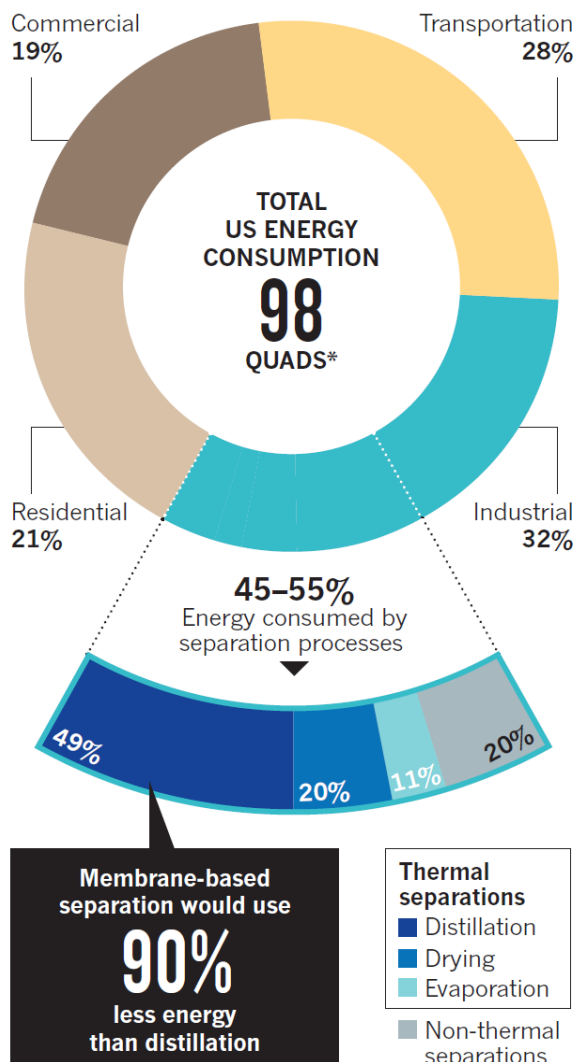
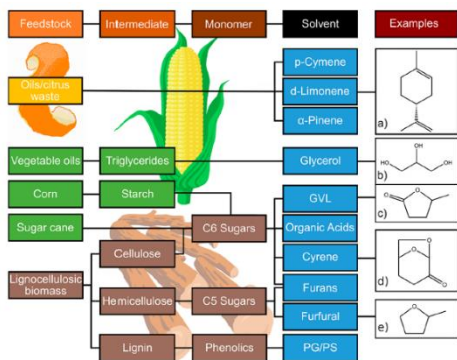


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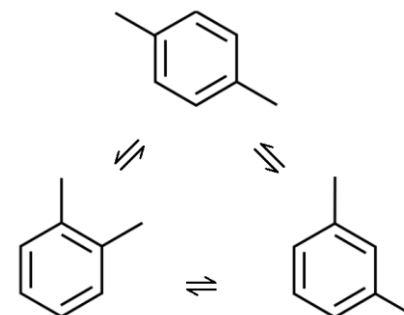
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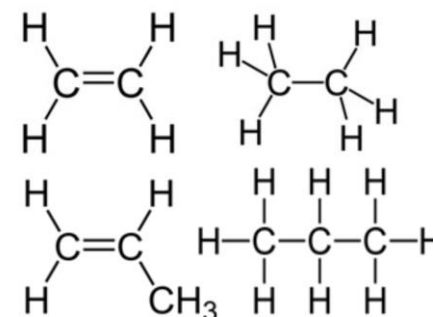
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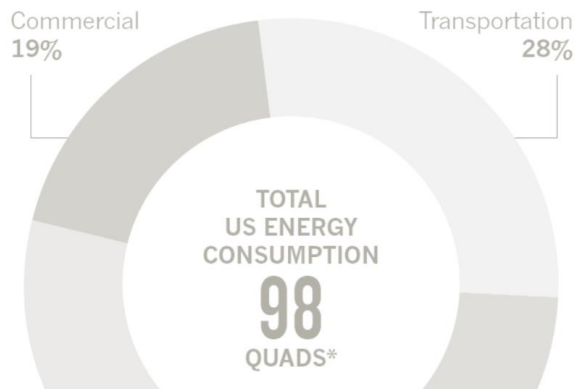
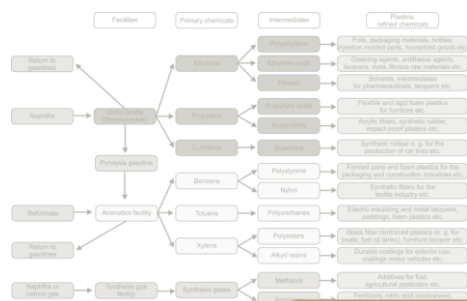
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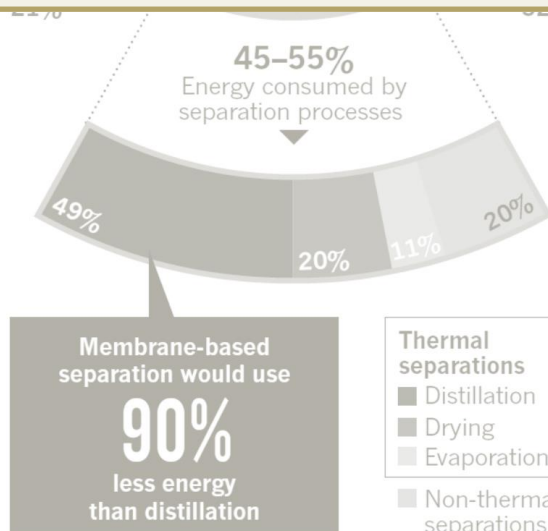
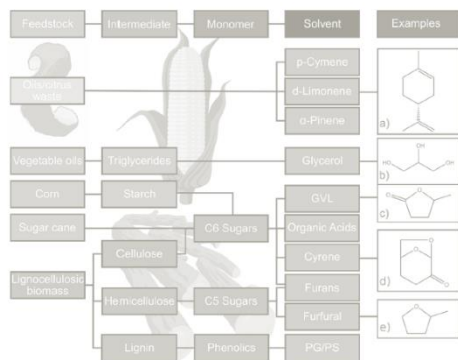
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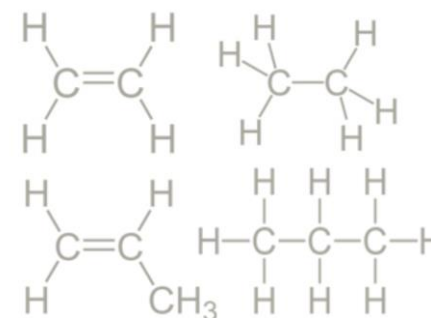
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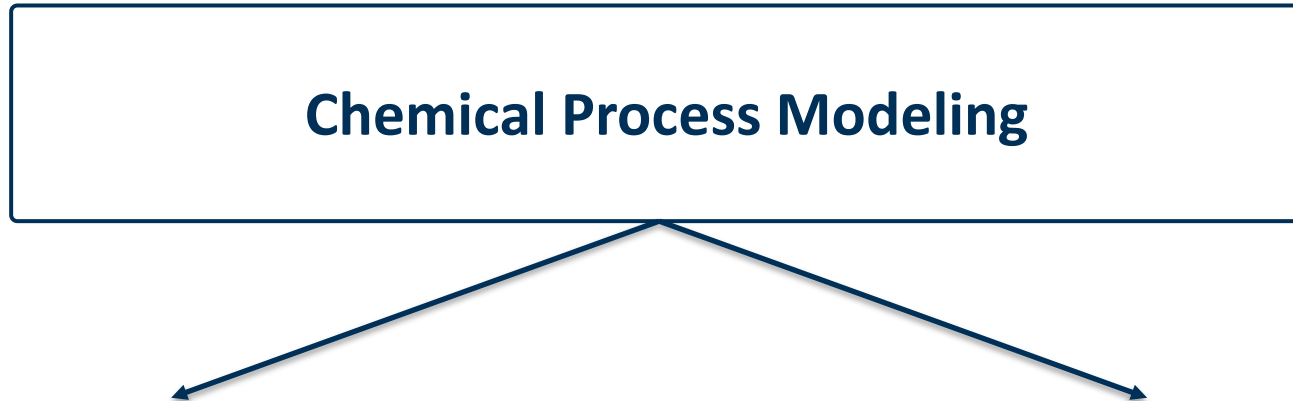
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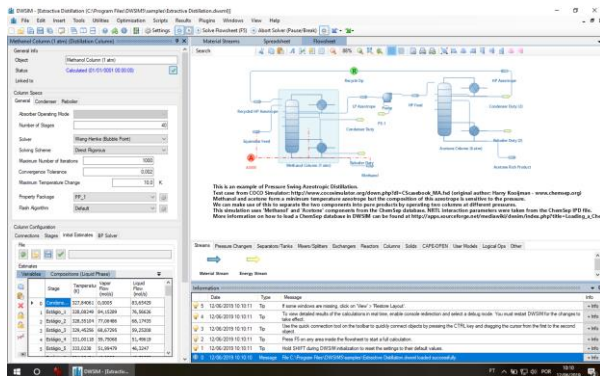
Standardized Interoperability – CAPE-OPEN



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Chemical Process Modeling

Process Modeling Environment (PME)

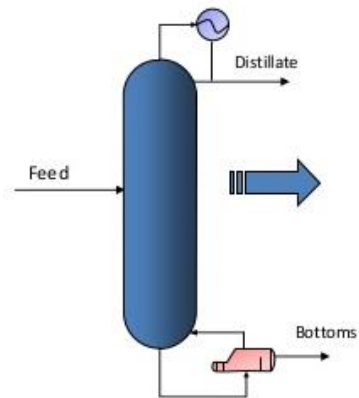
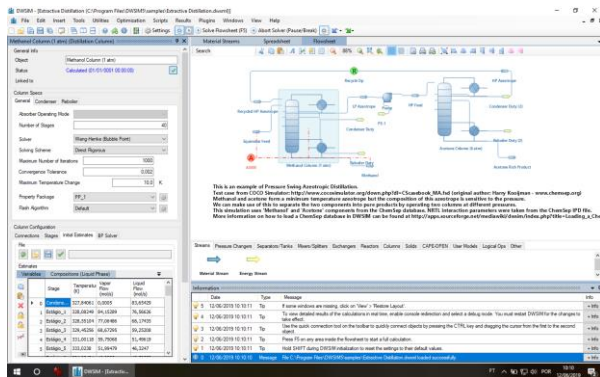


Standardized Interoperability – CAPE-OPEN

Chemical Process Modeling

Process Modeling
Environment (PME)

Process Modeling
Component (PMC)



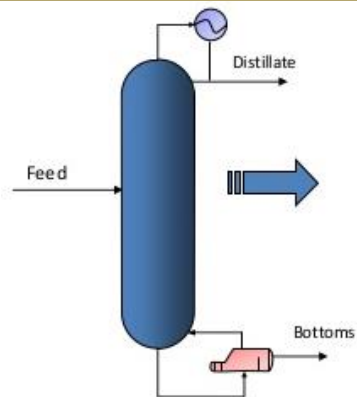
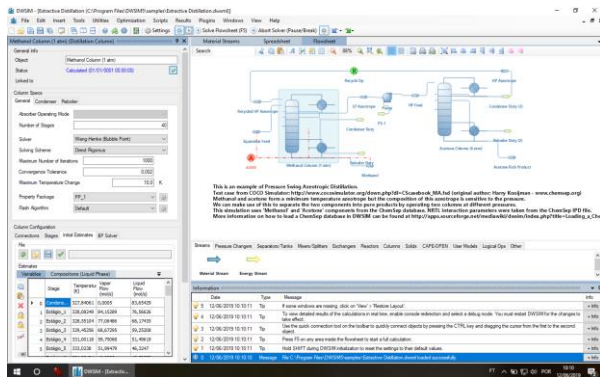
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Chemical Process Modeling

Process Modeling
Environment (PME)



Process Modeling
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Our Use Case

Chemical Process Modeling

Proprietary
Thermodynamic
Package Flowsheet

ExxonMobil

 **aspentech**



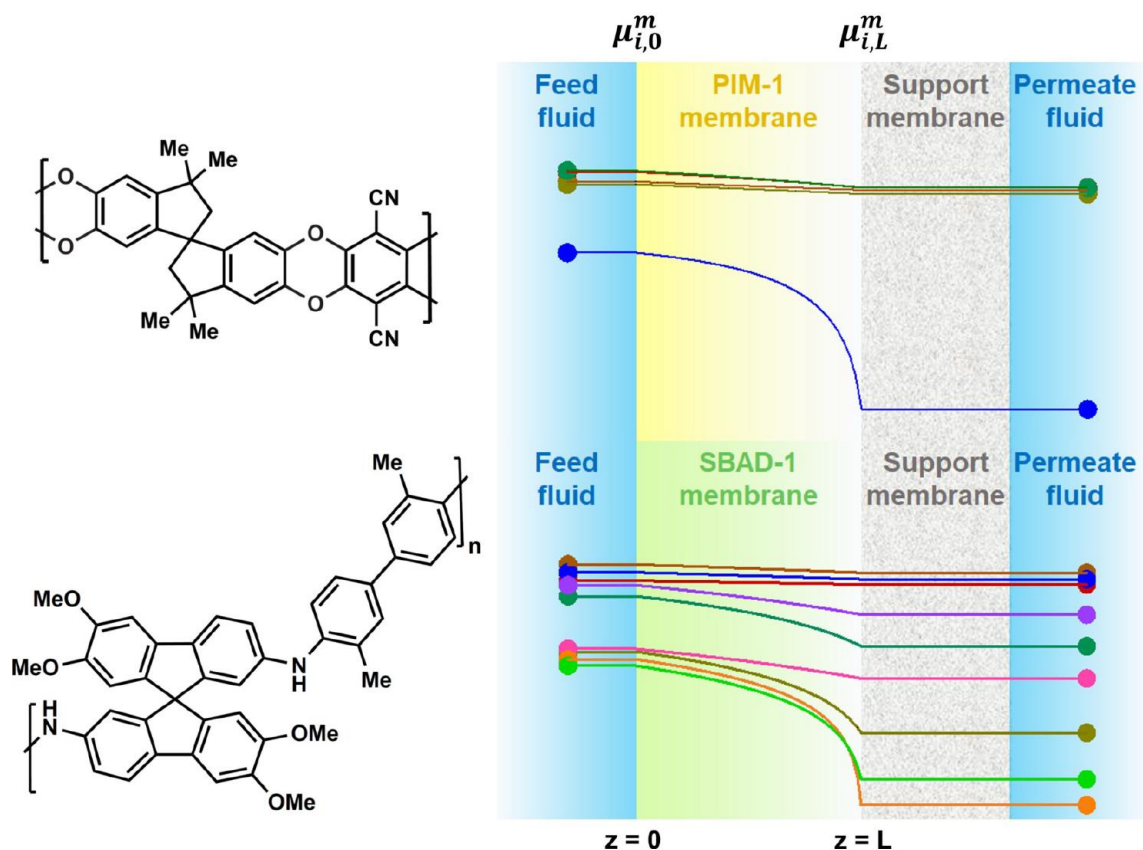
Complex Hydrocarbon
Mixture Polymeric
Membrane Simulation



amsterCHEM
tailor-made engineering software solutions

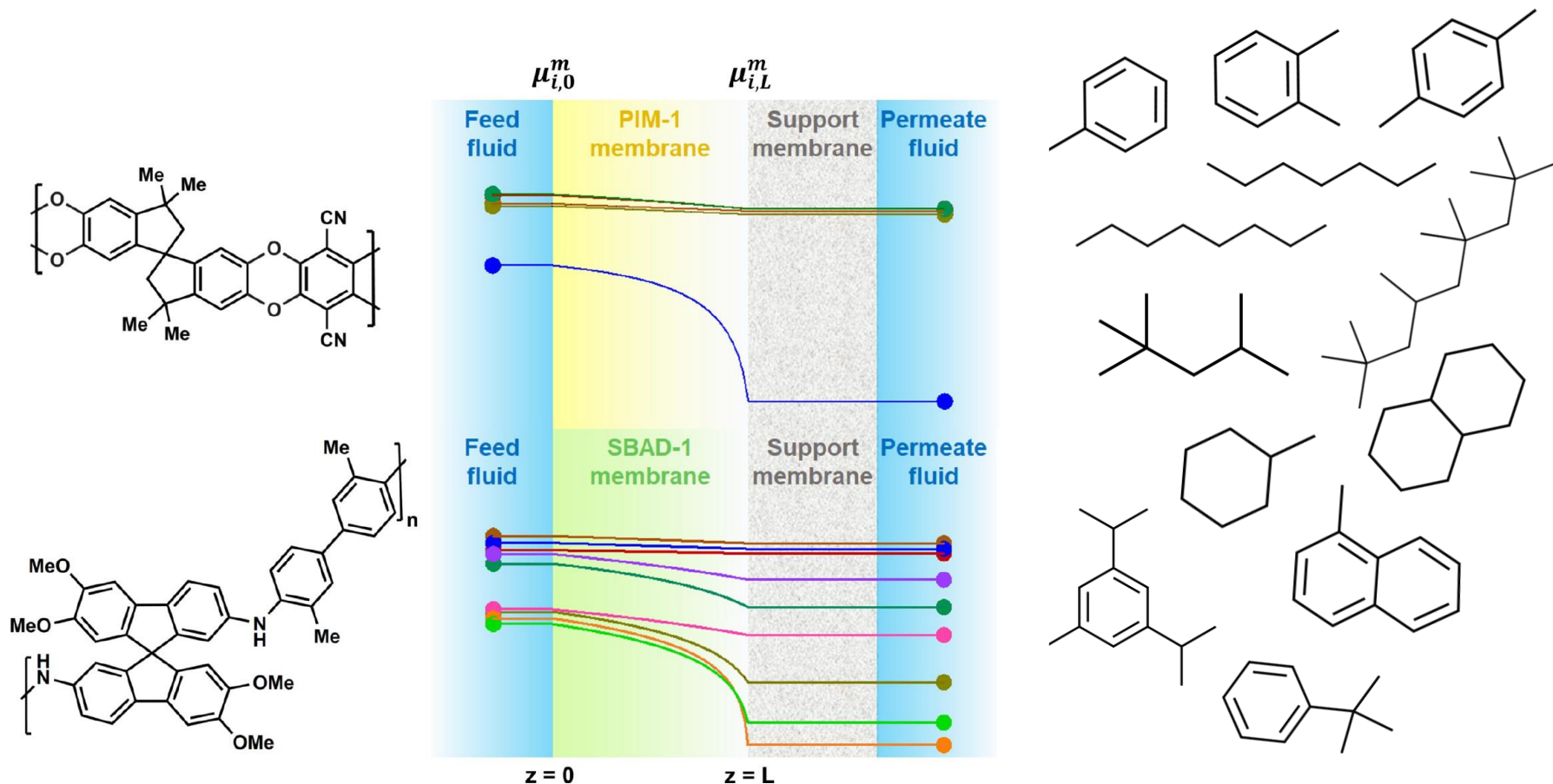
Our Application

For our experimental collaboration publication with Dr. Ryan Lively's group at Georgia Tech, we looked at 2 glassy polymer membrane materials and 3 complex mixtures⁵:



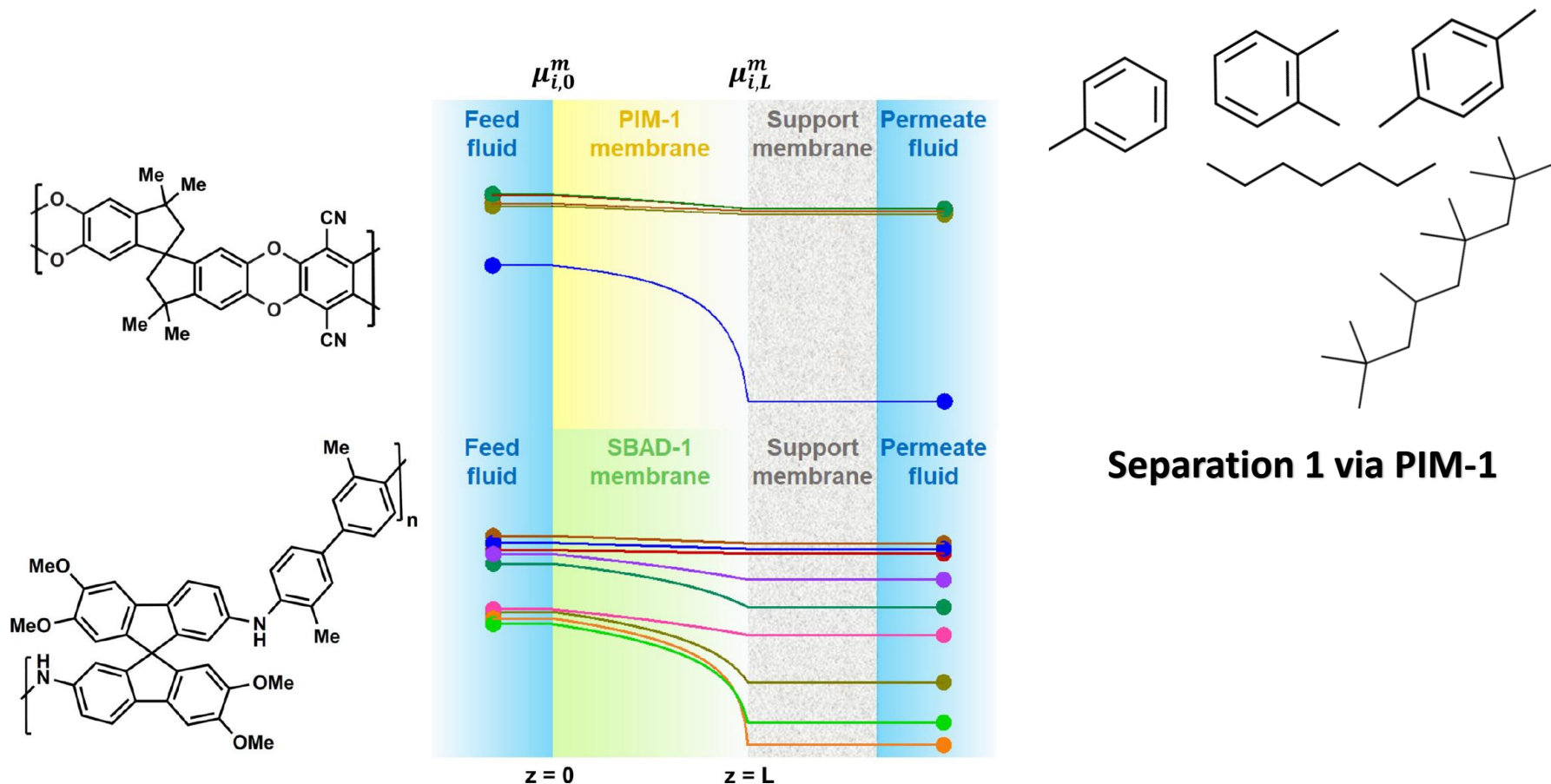
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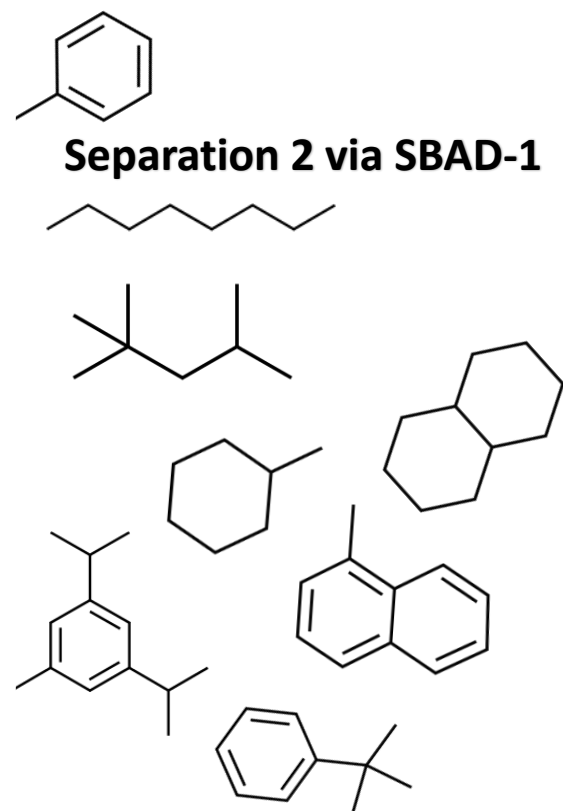
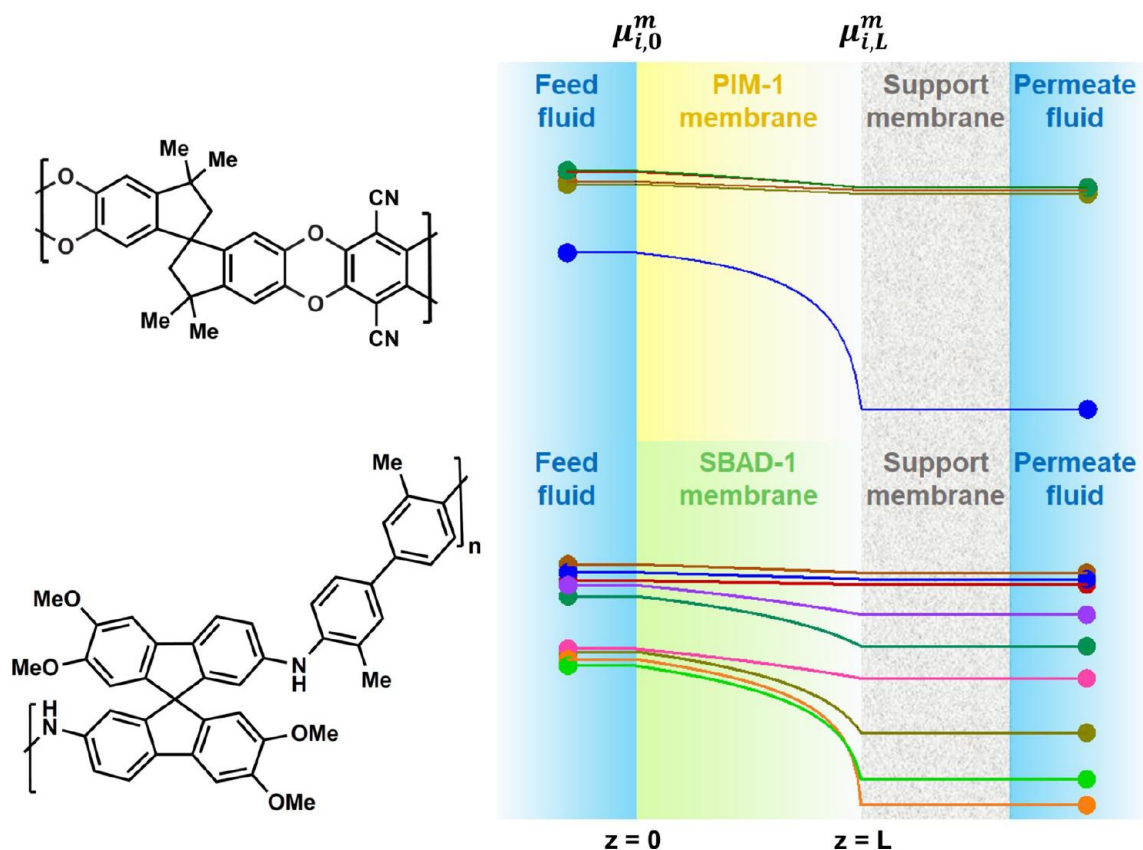
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Separation 1 via PIM-1

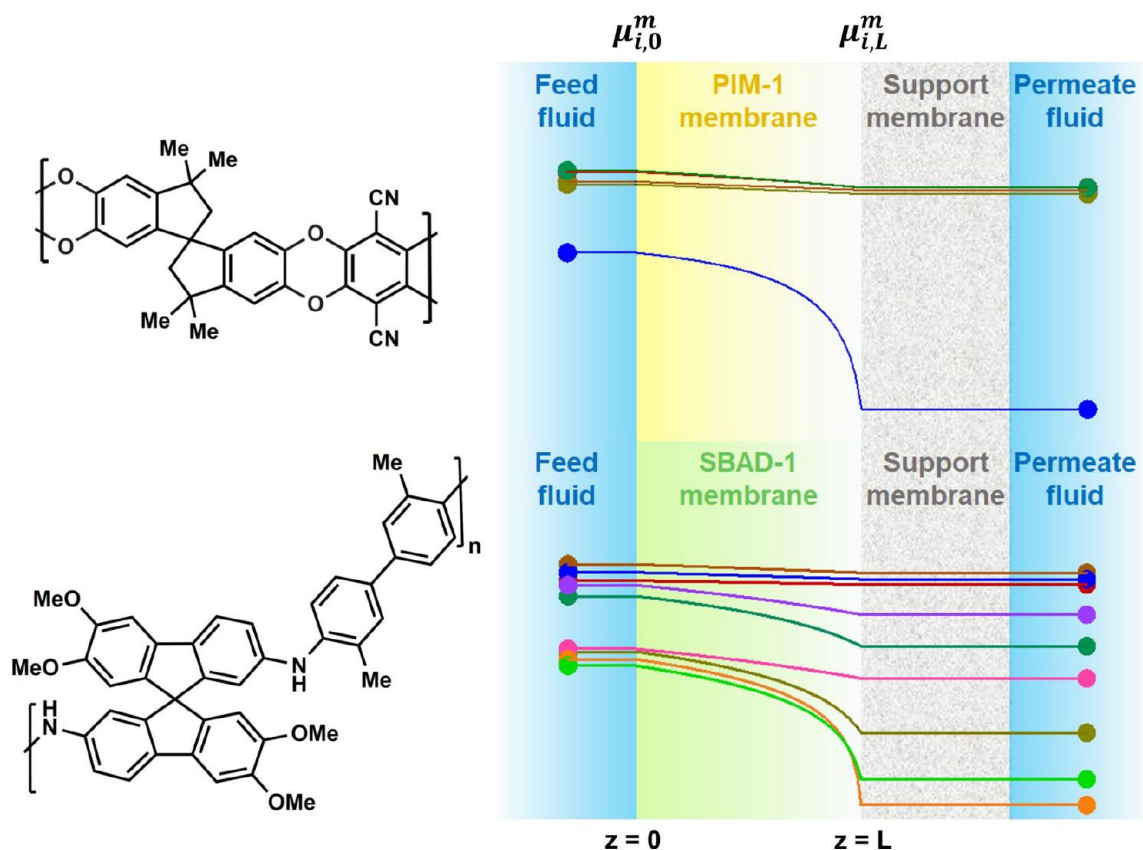
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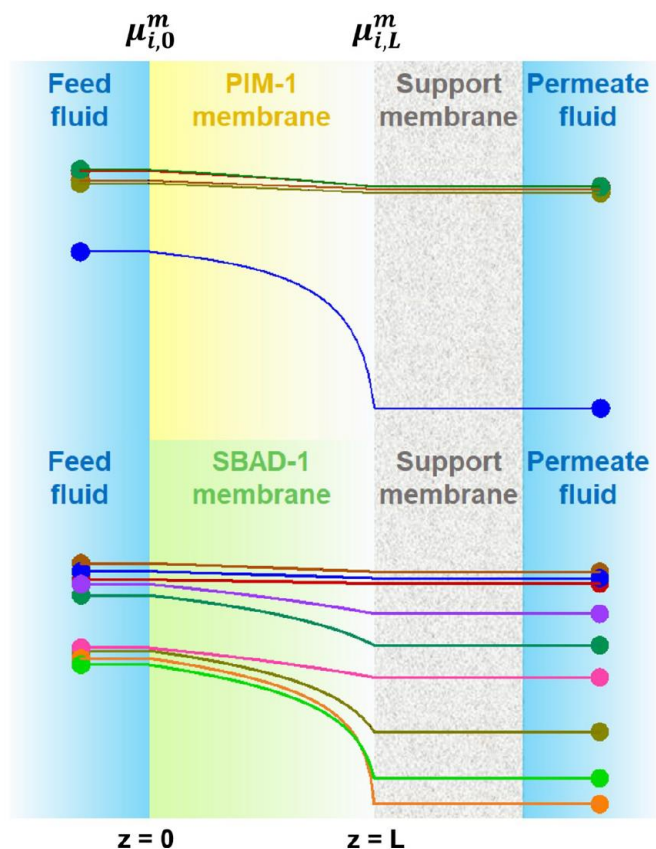
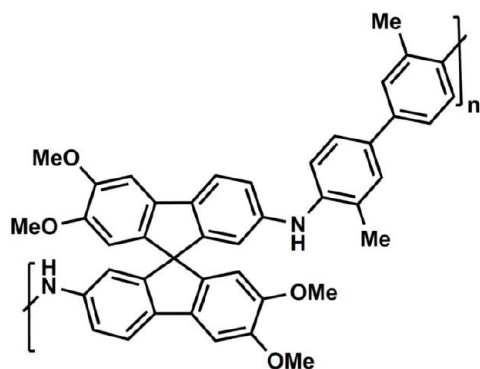
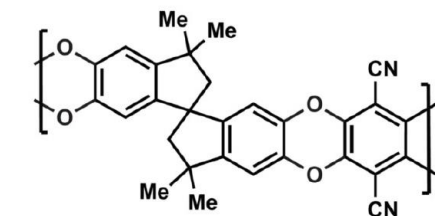
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Separation 3 via SBAD-1

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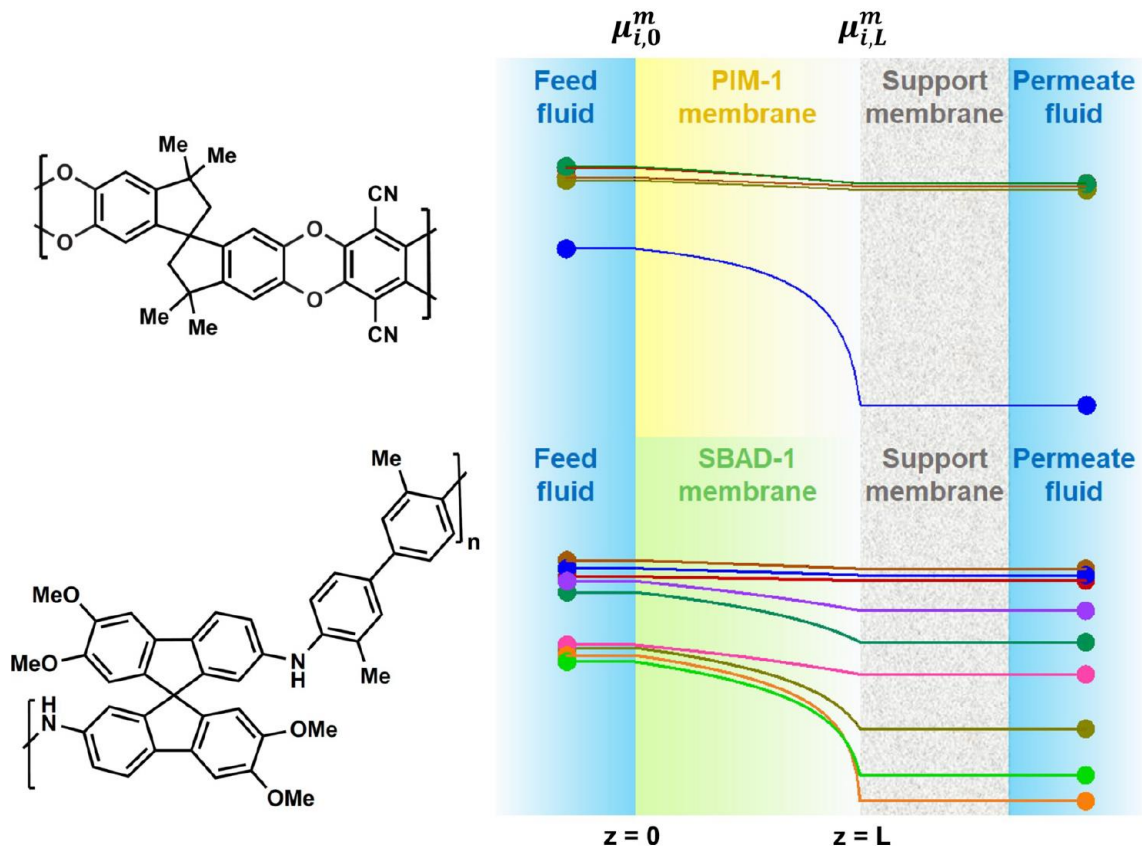
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This CAPE-OPEN tool allowed assessment of:
3 different membrane sorption models
5 different diffusion scenarios

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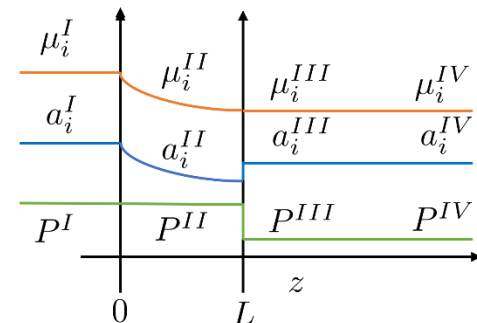
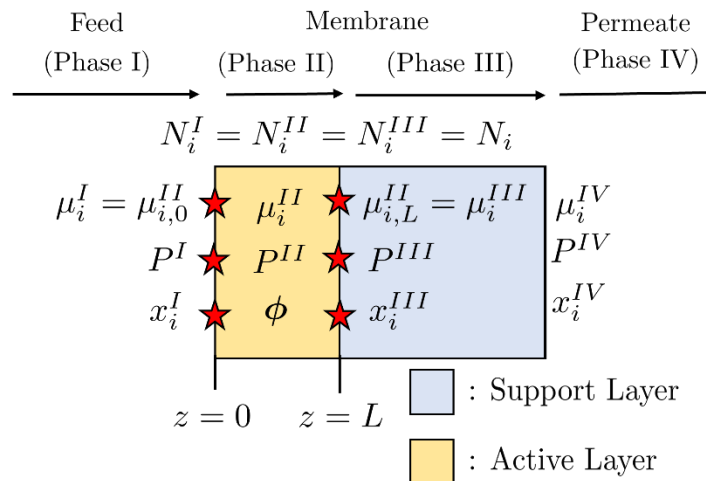
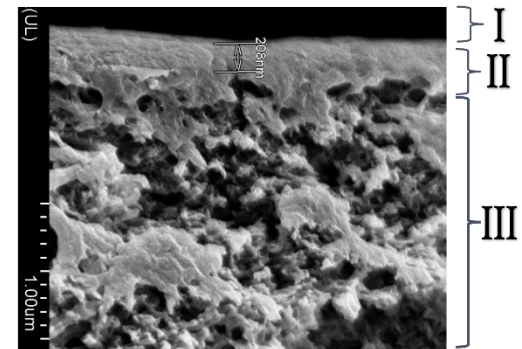
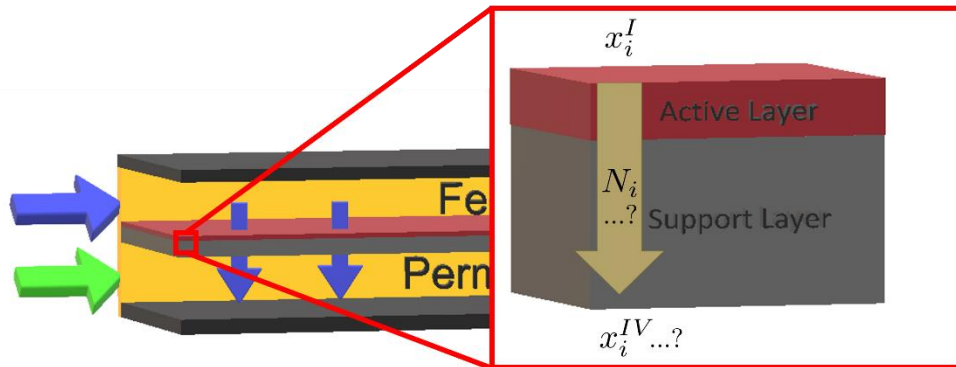
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3 different membrane
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*For glassy polymers
we proposed:
1 sorption model
2 diffusion models*

Our Membrane Simulation

Utilizing this software, we made a custom PMC for industrial membrane modules.

- First, we need to set up the local transport problem through an asymmetric membrane layer¹



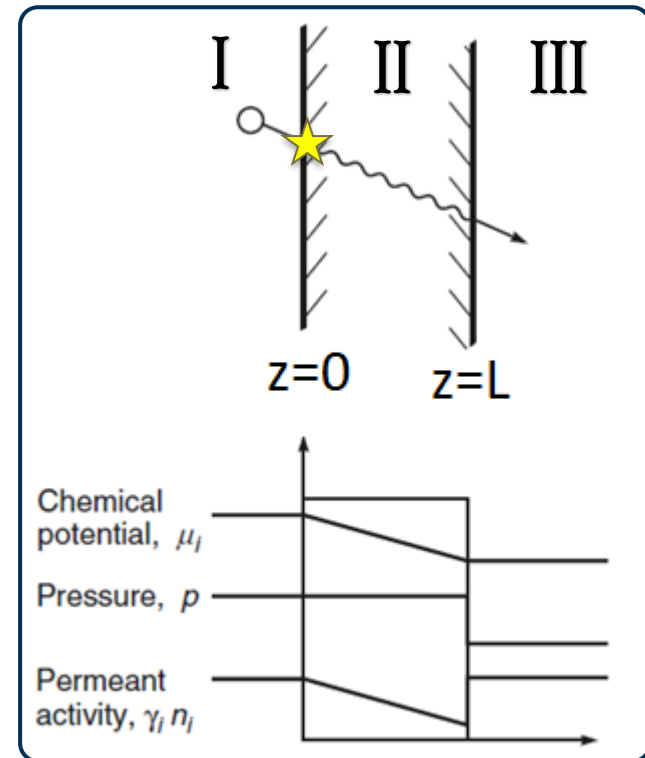
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- A. thermodynamic equilibrium (sorption) between phase (I) and (II)



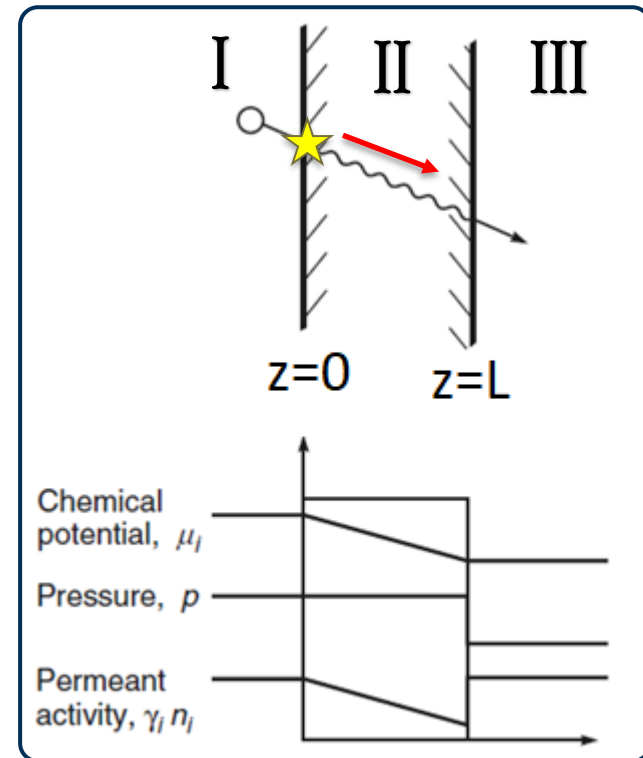
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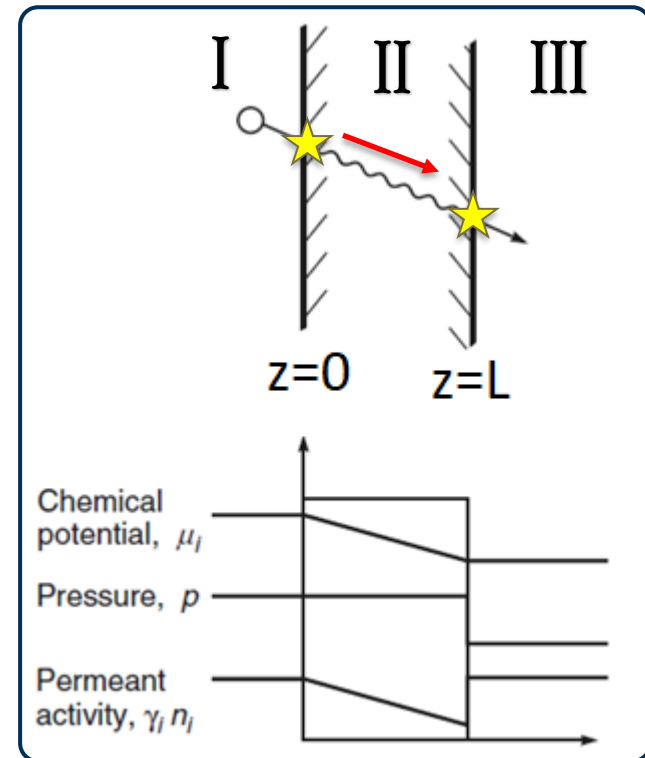
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- diffusion through phase (II)
- sorption between phase (II) and (III)



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- Then, we need to picture the full system of equations for the three-step sorption-diffusion model¹

Sorption-Diffusion Step A

$$0 = g_i^I(\gamma_i^I, \mathbf{x}^I, \mathbf{s}, T, P^I), \quad i = 1, 2, \dots, n$$

$$\hat{f}_{i,0}^{II} = \gamma_{i,0}^I x_i^I f_i^\circ, \quad i = 1, 2, \dots, n$$

$$0 = w_i^{II}(\mathbf{f}^{II}, \phi_0, \mathbf{s}, T, P^{II}), \quad i = 1, 2, \dots, n$$

$$\sum_{j=1}^{n+1} \phi_{j,0} = 1$$

Sorption-Diffusion Step B

$$\frac{d\phi_{1:n}}{dz} = -\mathbf{\Gamma}^{-1}(\phi, \mathbf{f}^{II}, \mathbf{s}) \mathbf{B}(\phi) \mathbf{x}^{III} N_{tot}^{V*}$$

$$\frac{d\phi_{n+1}}{dz} = -\sum_{j=1}^n \frac{d\phi_j}{dz}$$

$$\mathbf{w}(\phi, \mathbf{f}^{II}) = 0$$

Sorption-Diffusion Step C

$$0 = g_i^{III}(\gamma_i^{III}, \mathbf{x}^{III}, \mathbf{s}, T, P^{III}), \quad i = 1, 2, \dots, n$$

$$\hat{f}_{i,L}^{II} = \gamma_{i,L}^{III} x_i^{III} f_i^\circ \eta, \quad i = 1, 2, \dots, n$$

$$0 = w_i^{II}(\mathbf{f}^{II}, \phi_L, \mathbf{s}, T, P^{II}), \quad i = 1, 2, \dots, n$$

$$\sum_{j=1}^n x_j^{III} = 1$$

Known variables:

$$(\mathbf{x}^I, L, T, P^I, P^{II}, P^{III}, \mathbf{s}, \mathbf{D})$$

Unknown variables:

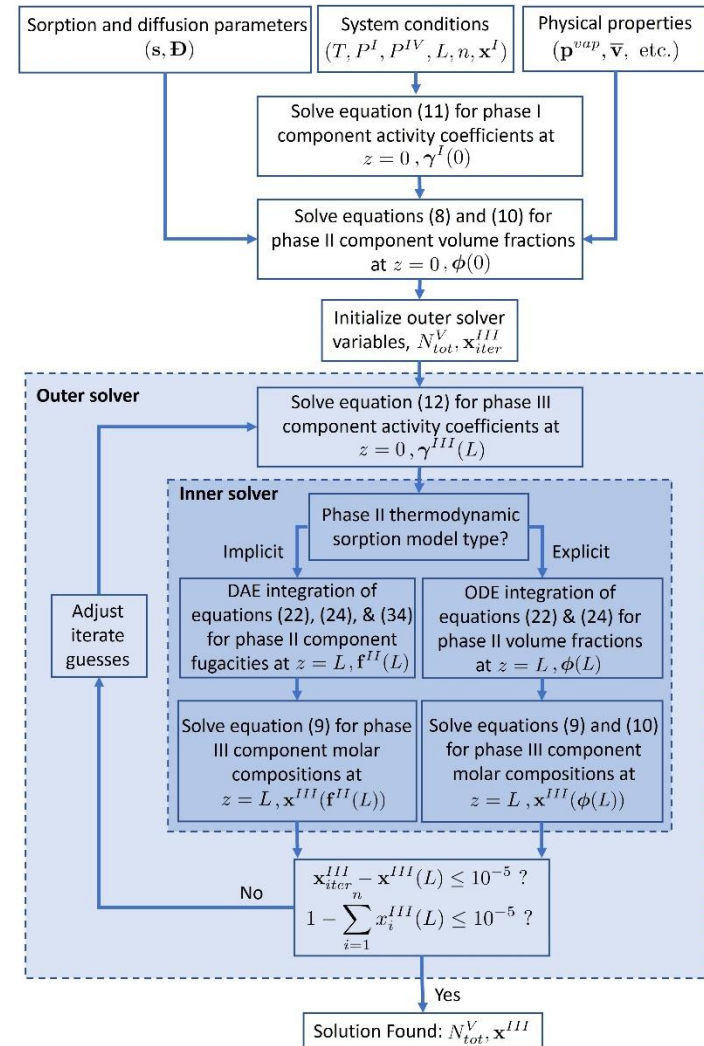
$$(\gamma^I, \gamma^{III}, \mathbf{f}_0^{II}, \mathbf{f}_L^{II}, \phi_0, \phi_L, \mathbf{x}^{III}, N_{tot}^{V*})$$

$$\begin{aligned} \text{DoF: } & 4n + 3(n + 1) \text{ equations} \\ & -4n + 3(n + 1) \text{ unknowns} \\ & = 0 \text{ DoF} \end{aligned}$$

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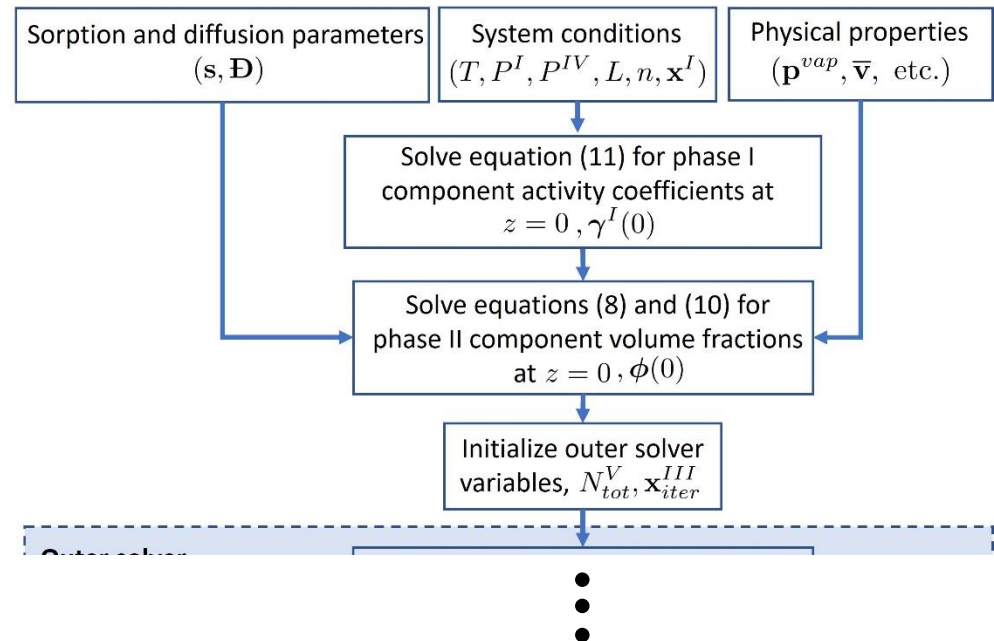
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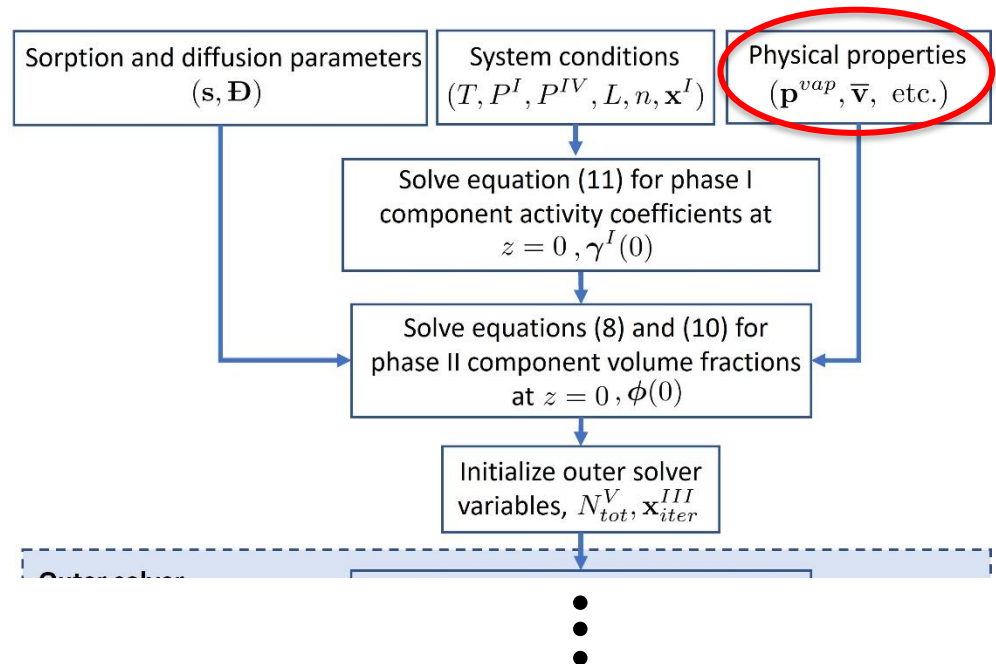


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*Pure component properties
evaluation/lookup for all
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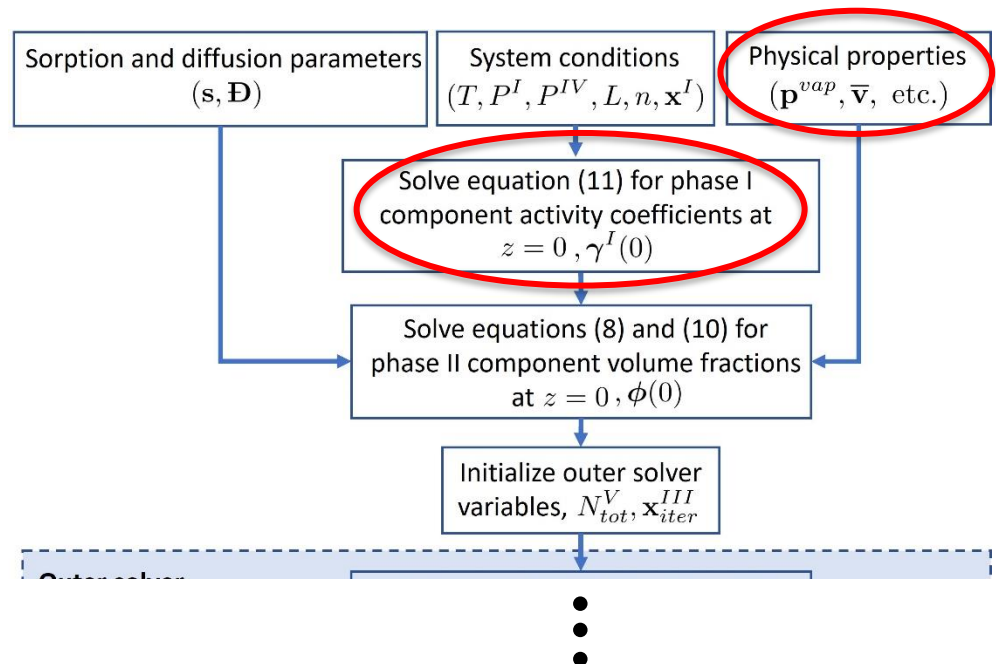
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*Sorption-Diffusion Step A
requires evaluation of
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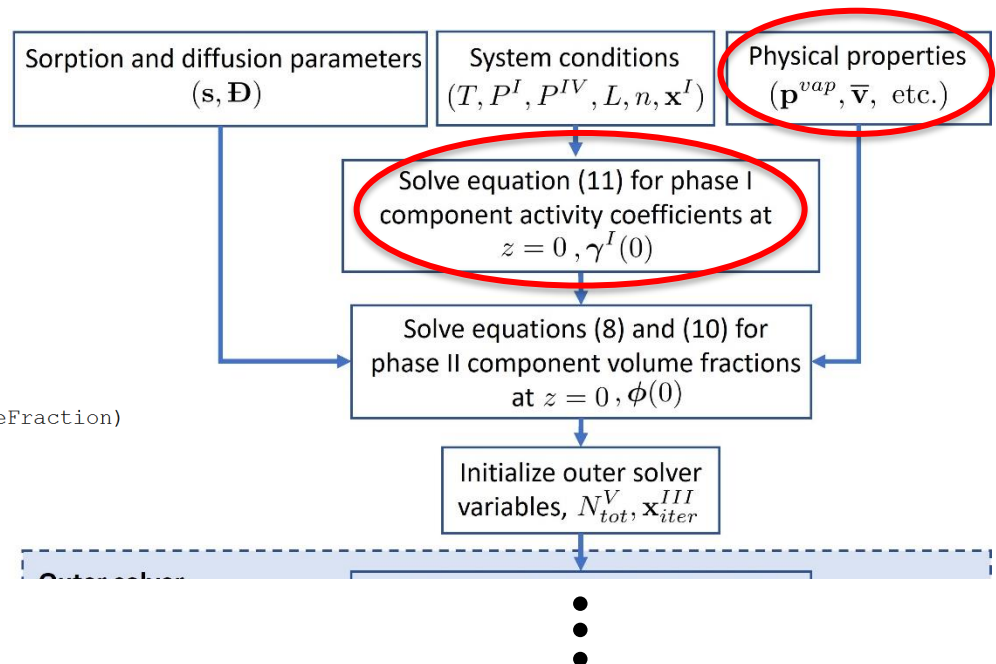
getSinglePhaseProperty

getSinglePhaseProperty is used to retrieve single phase mixture properties.

Syntax

`value=getSinglePhaseProperty(propName,phaseName,T,P,moleFraction)`

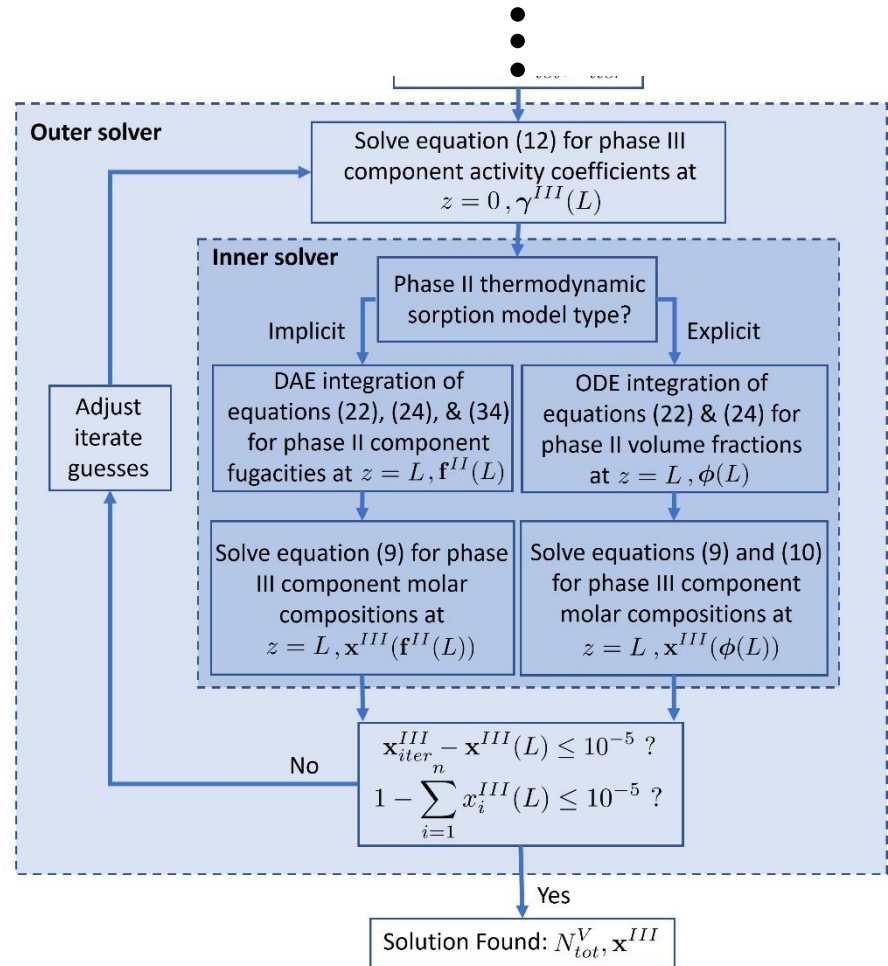
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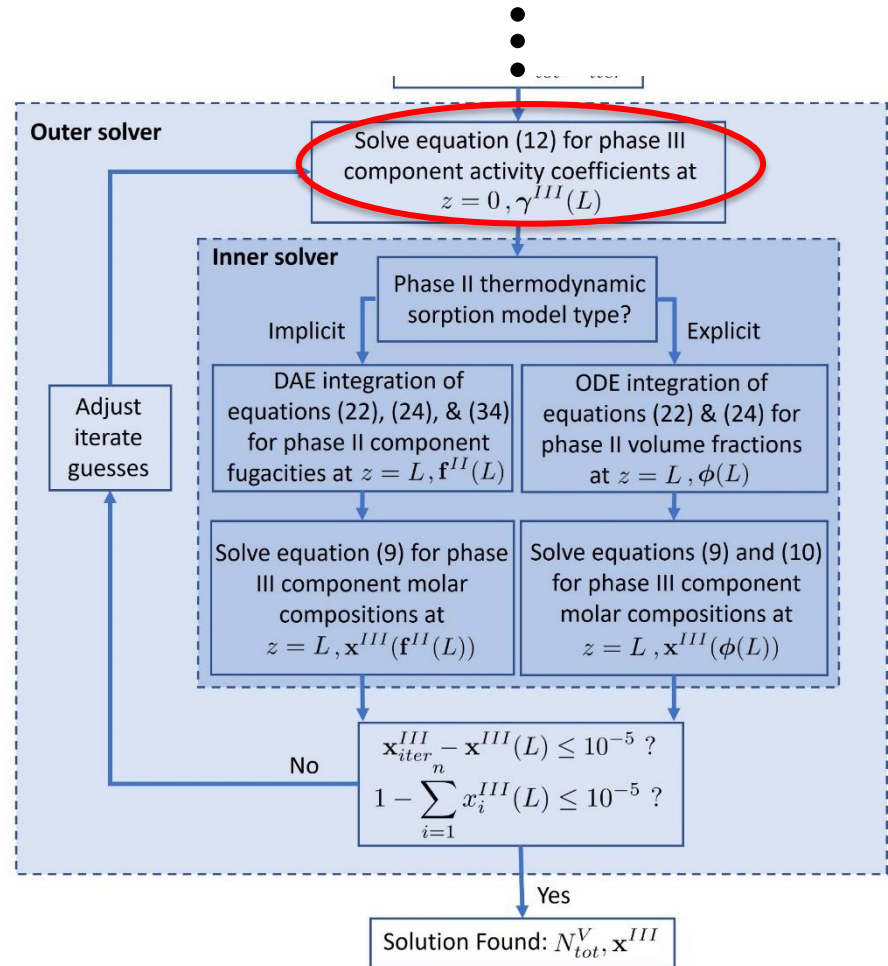


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Sorption-Diffusion Step C requires evaluation of activity model in phase III



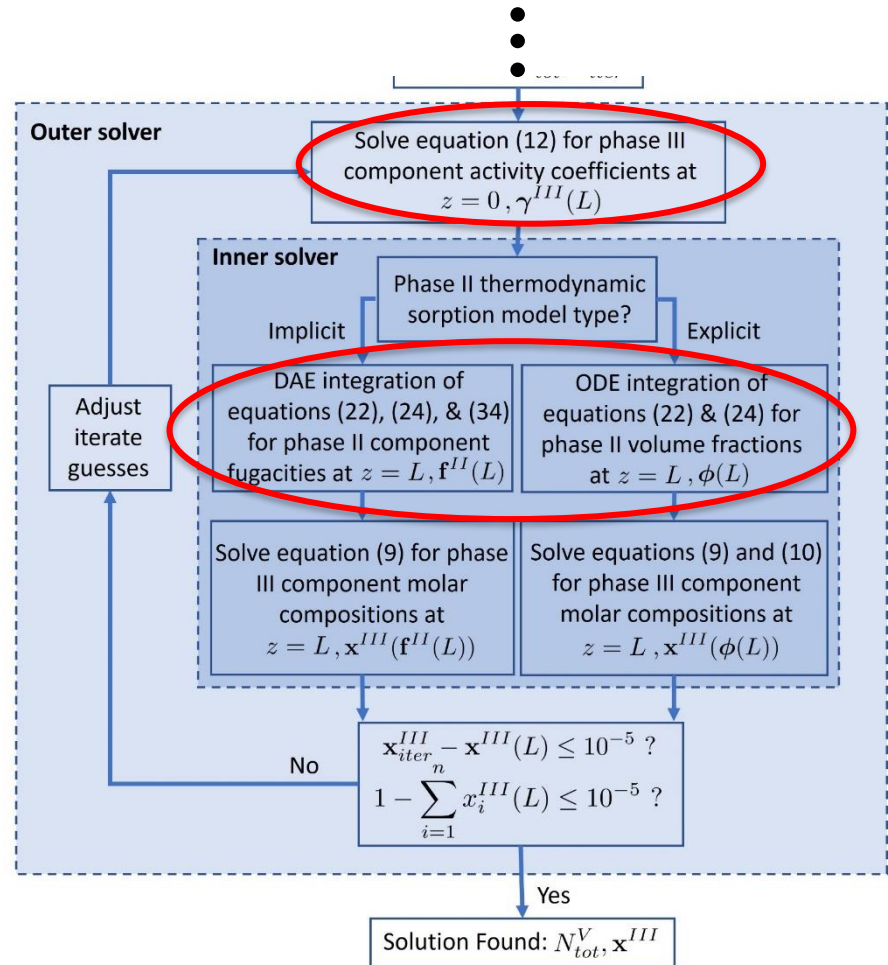
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Sorption-Diffusion Step B uses
pure component fugacities to
evaluate phase II component
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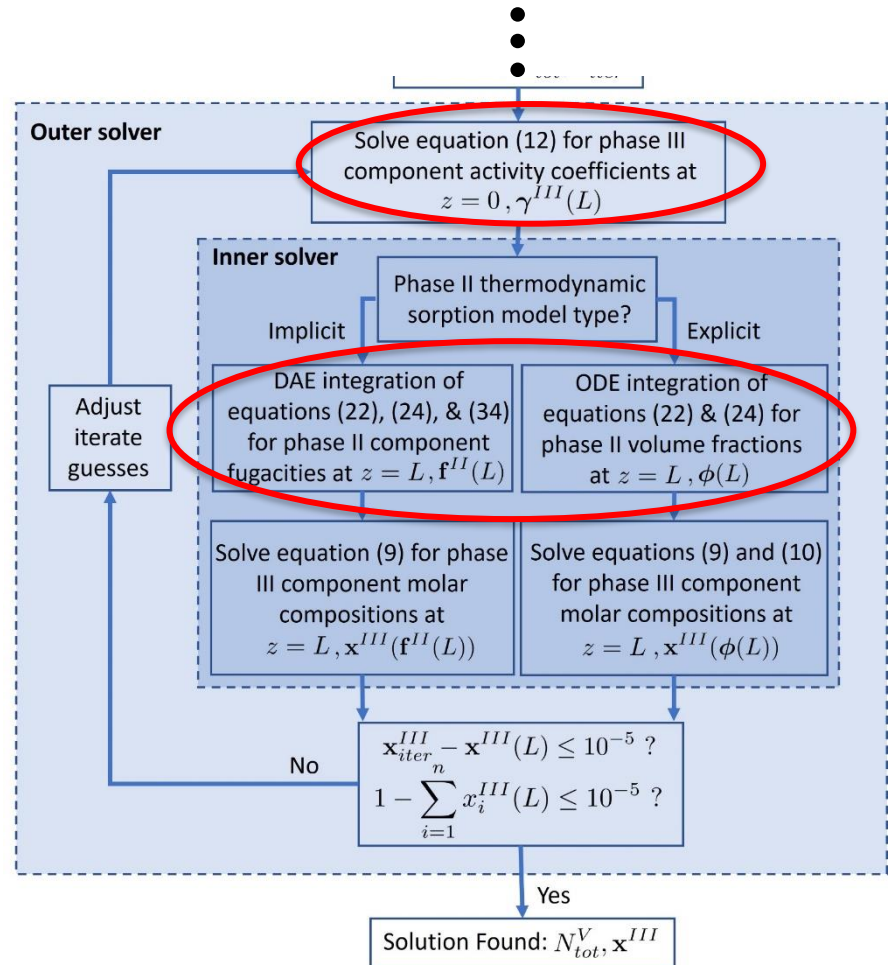
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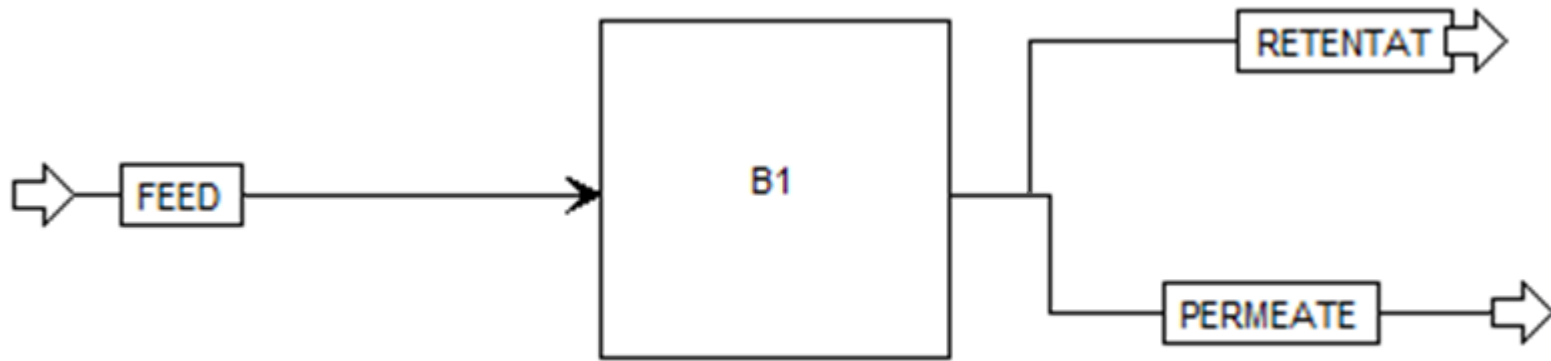
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Using AmsterCHEM's Software

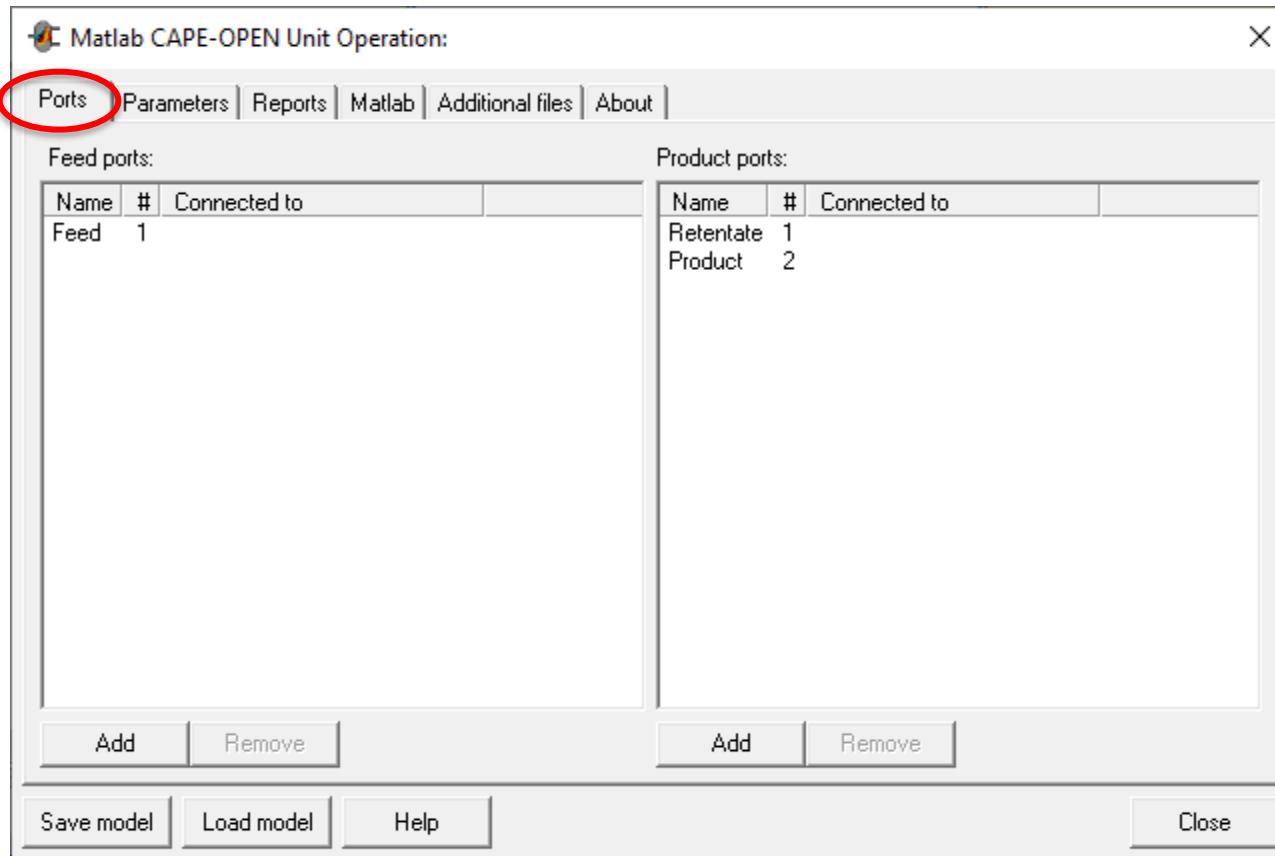
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Matlab Unit Operation

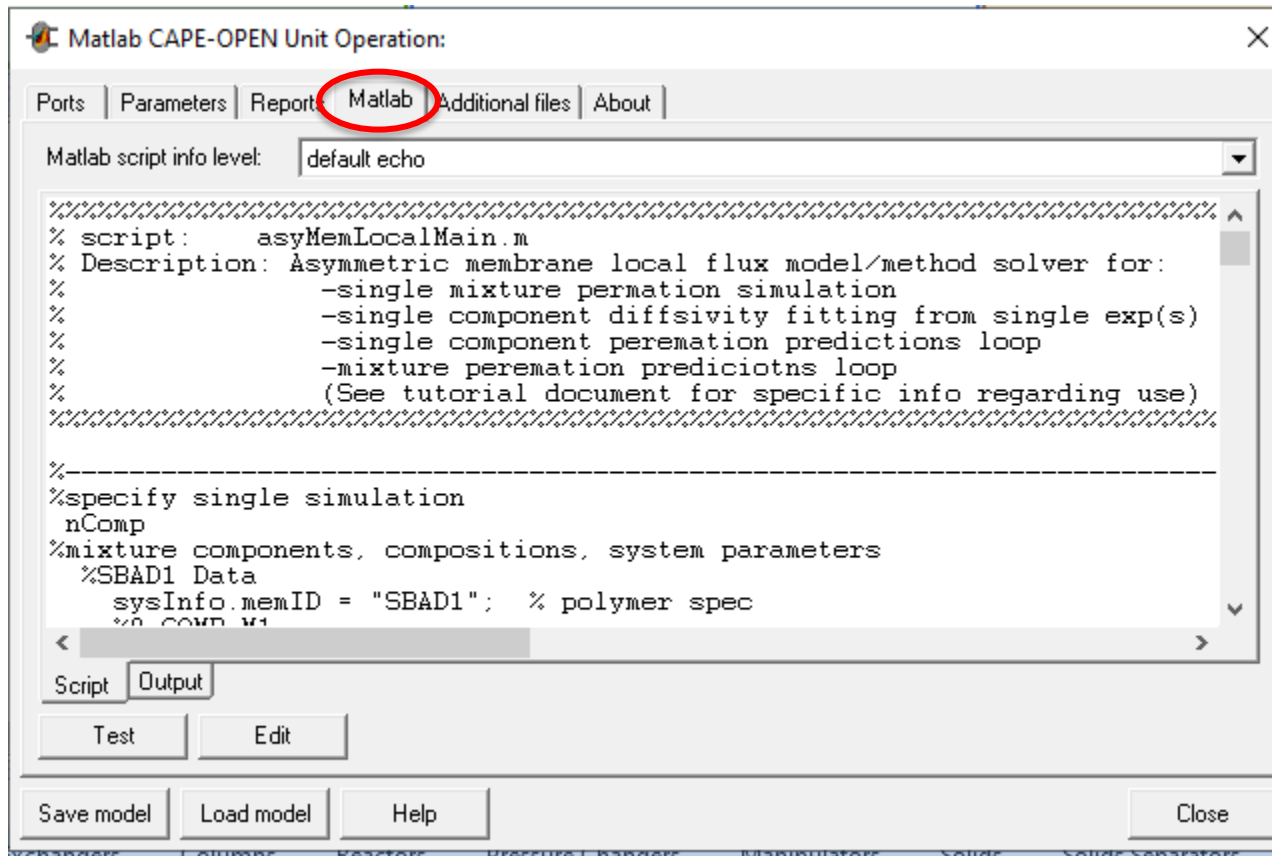
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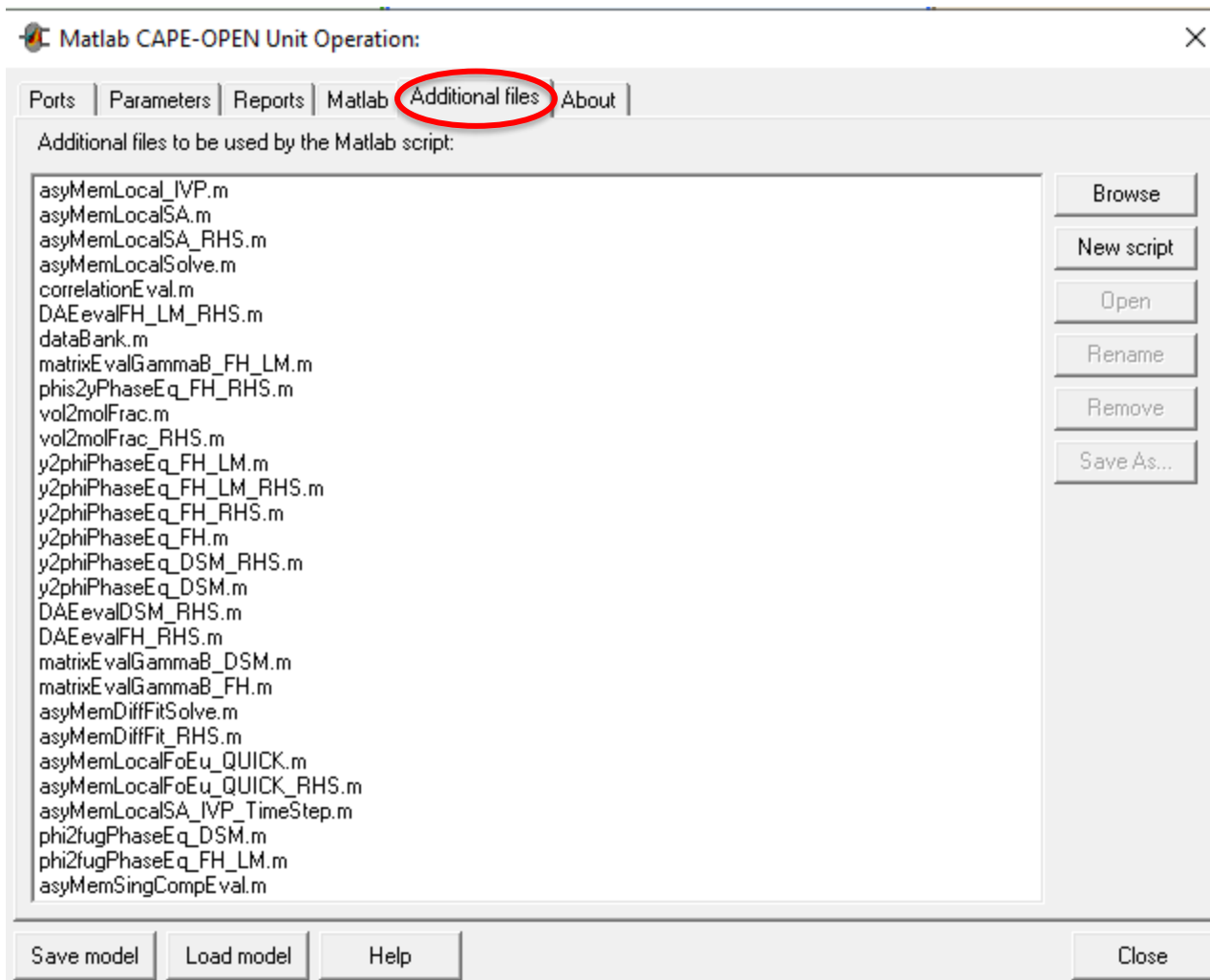
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**Input mixture component,
membrane and model selection**

```
%mixture components, compositions, system parameters
%SBAD1 Data
sysInfo.memID = "SBAD1"; % polymer spec
%9 COMP M1
sysInfo.mixID = ["TOL","MCH","MNP","DEC","NOC","IOC","TBB","TPB","ICT"];
sysInfo.yf = [0.171;0.281;0.0199;0.107;0.221;0.15;0.0217;0.0158;0.013];
```

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%mixture components, compositions, system parameters
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```

- 2 membrane materials
- 12 components
- 3 sorption models
- 2 membrane diffusion models
- 2 cross-coupling diffusion models

Our Implementation

Custom complex hydrocarbon mixture permeation simulation based on pure component membrane sorption and diffusion properties.

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membrane and model selection**

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**Output all parameter matrices
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Proprietary thermodynamic mixture activity model parameters (Corporate Strategic Research, ExxonMobil Research and Engineering). **ExxonMobil**

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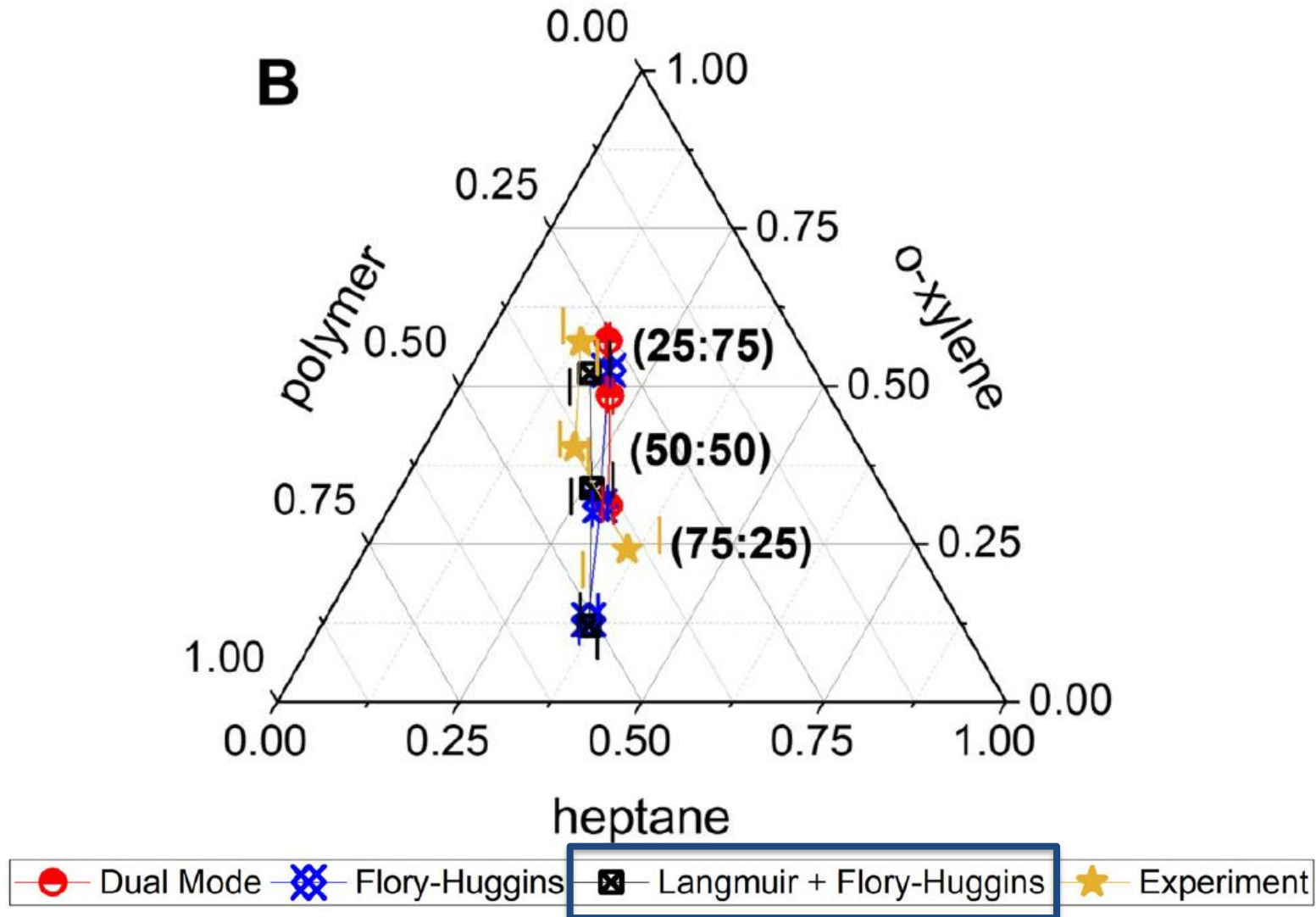
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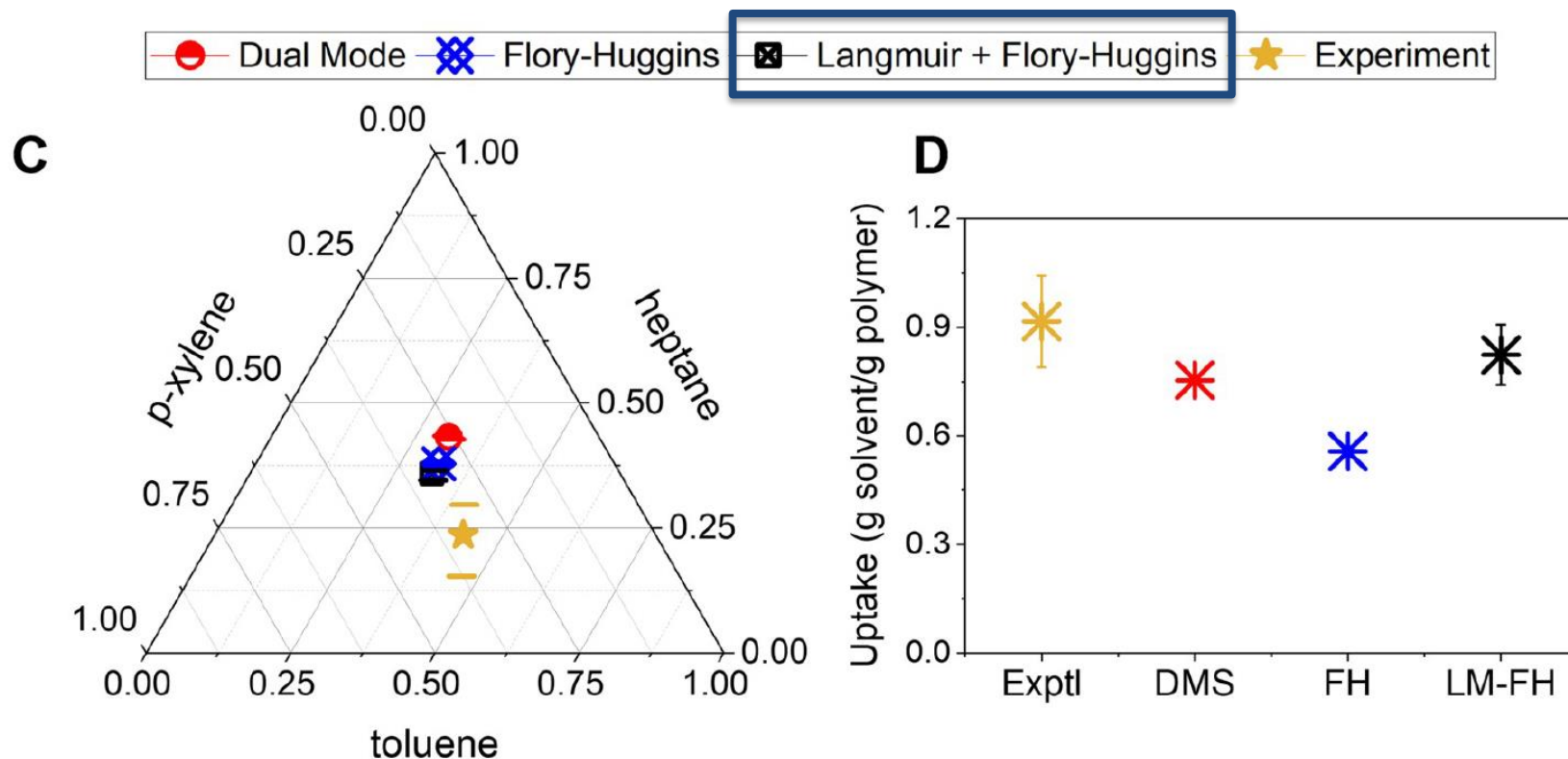
Ability to assess permeation predictions across different sorption/diffusion models and mixtures for validating what simulates a given application best⁵.

- **270** mixture permeation simulations across 3 mixtures
- **330** pure component permeation simulations across 12 components
- A handful of multicomponent sorption simulations

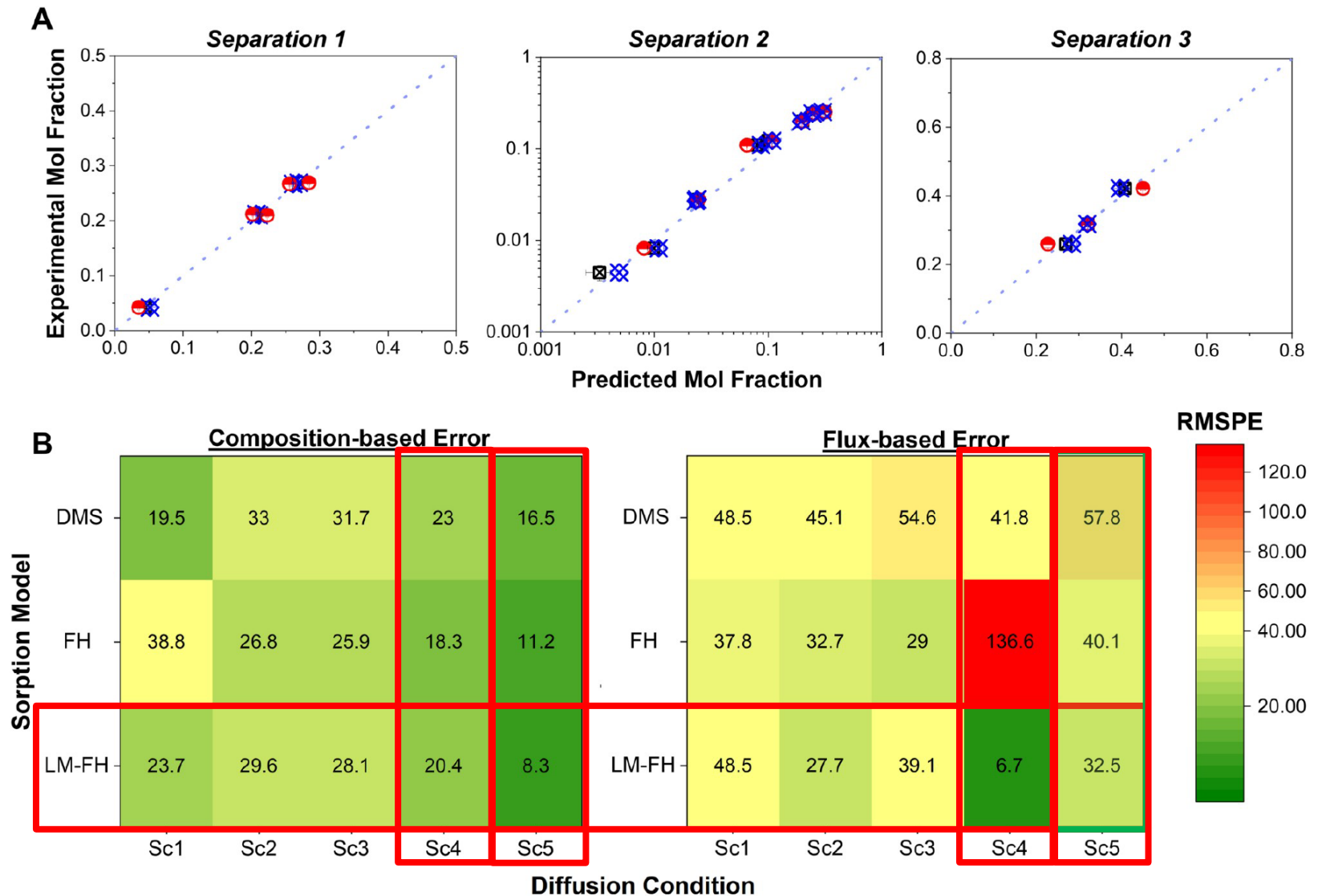
Predictions of Complex Mixture Sorption



Predictions of Complex Mixture Sorption



Predictions of Complex Mixture Permeation



Advantages and Challenges of AmsterCHEM's Software

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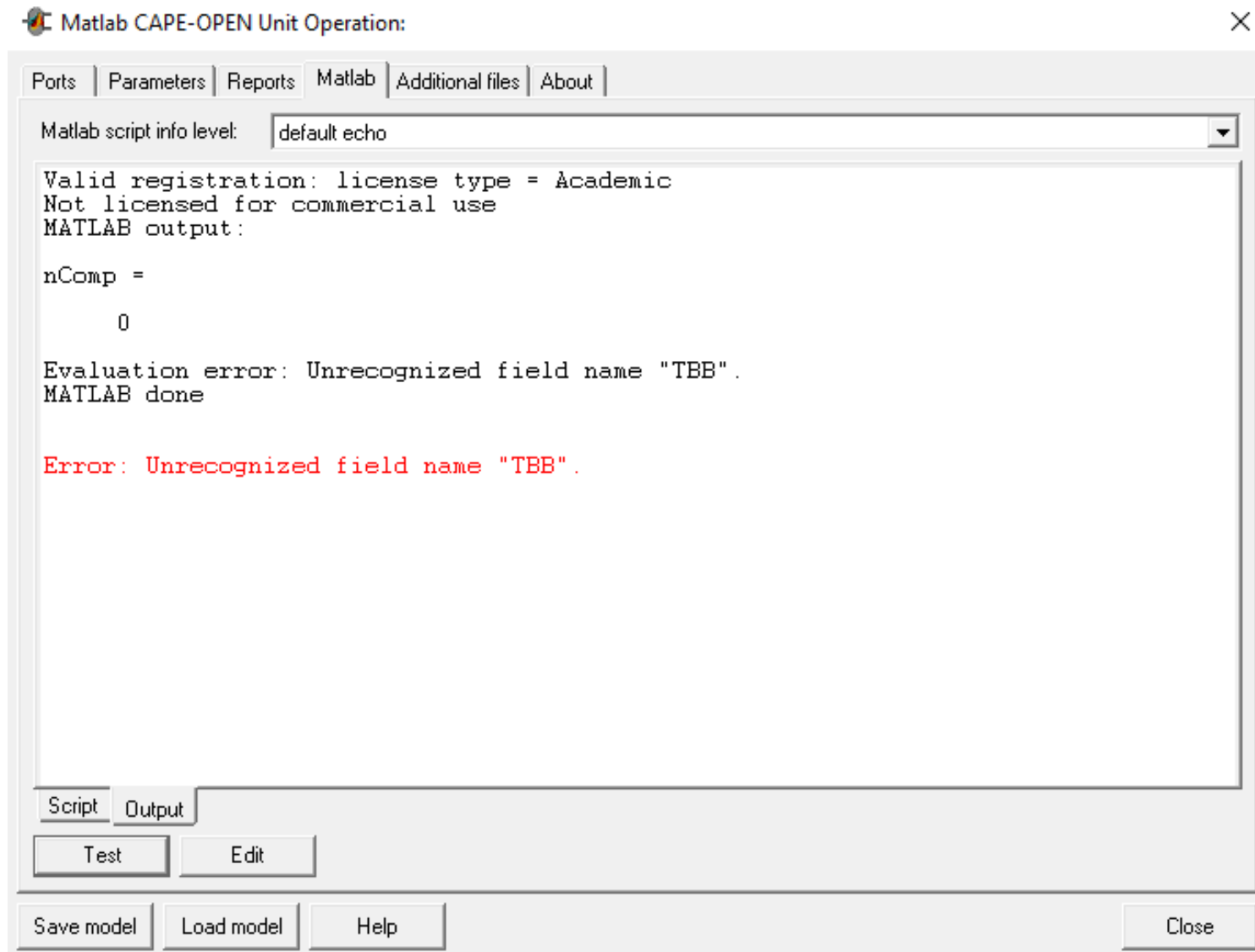
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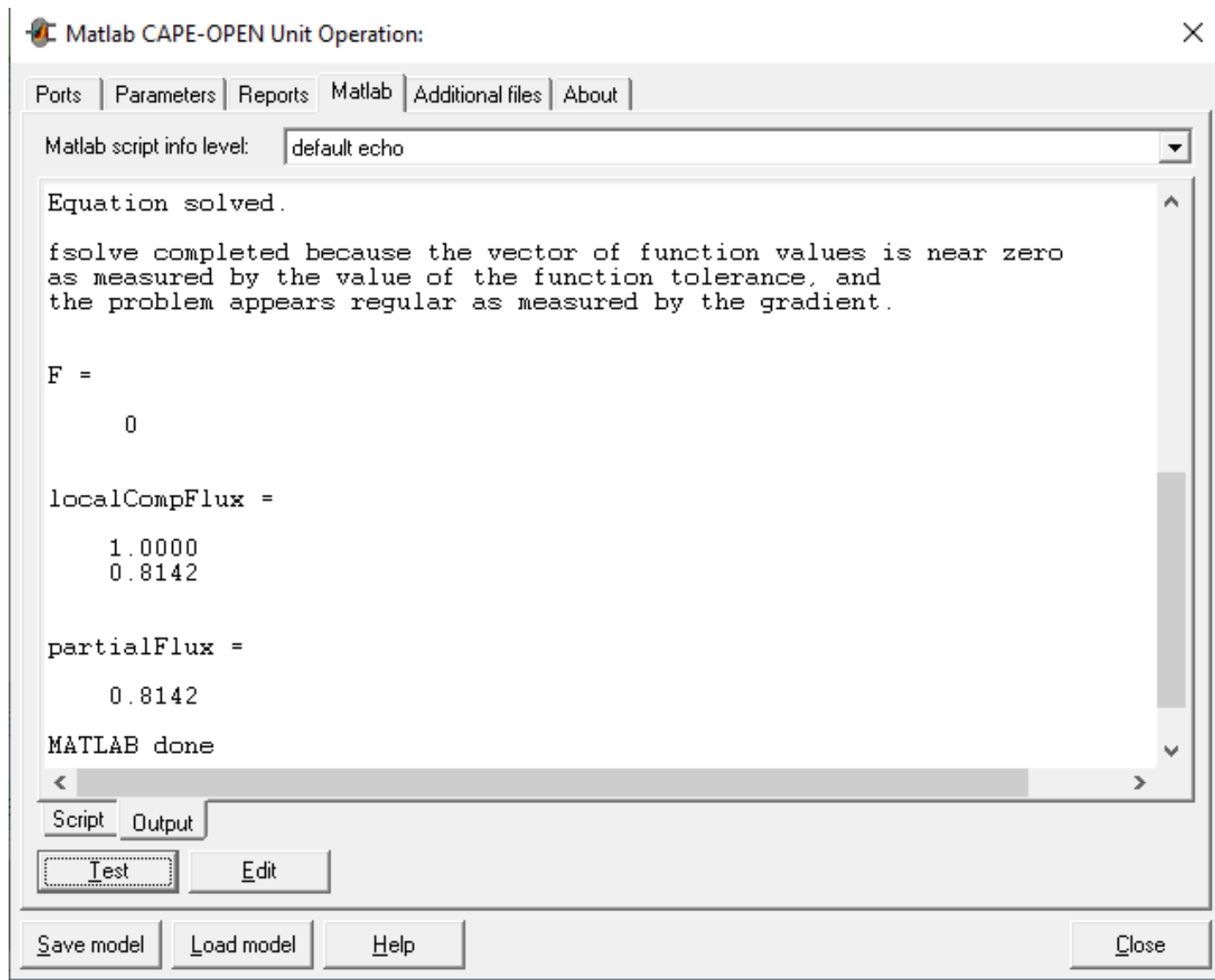
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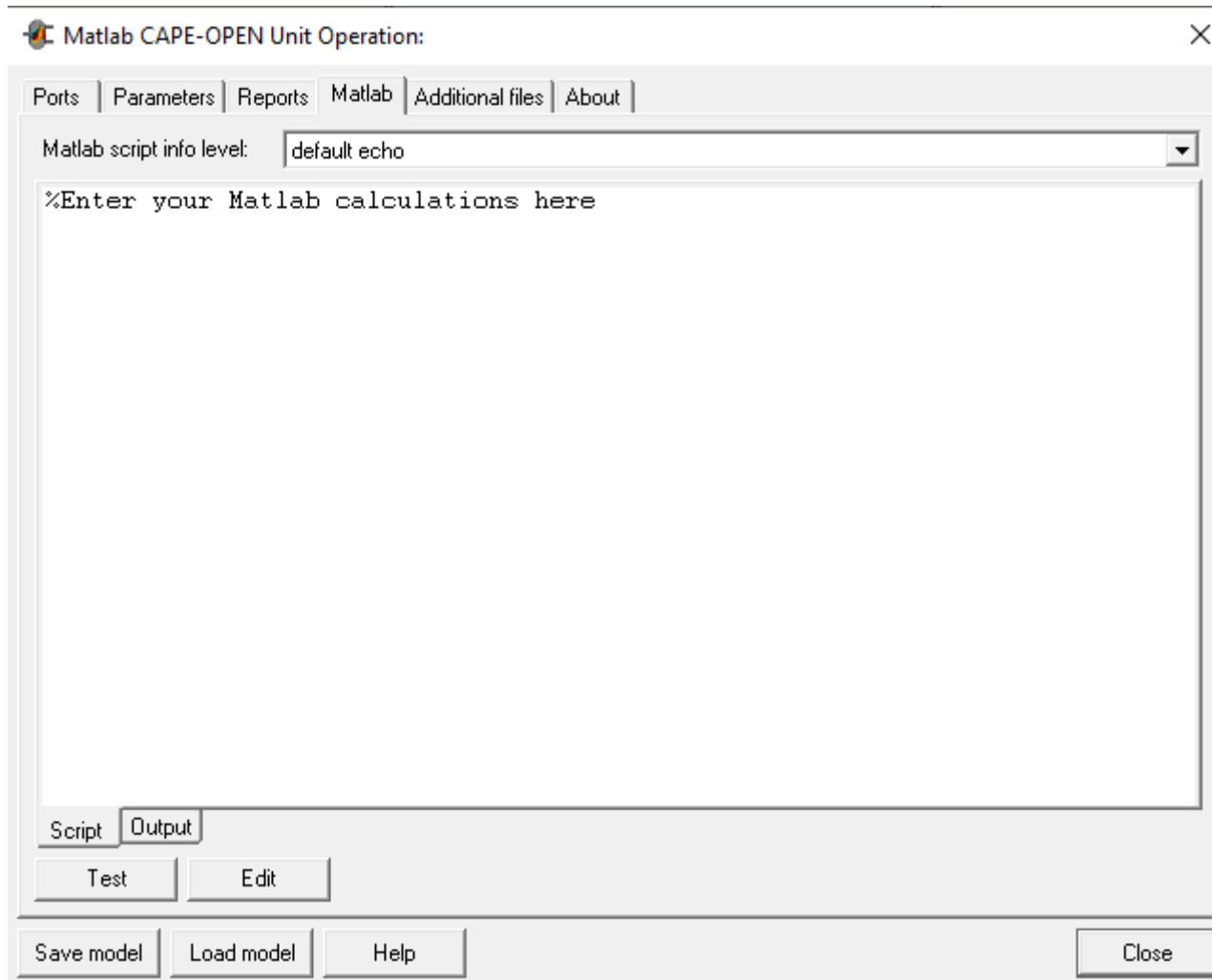
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The ability to save the MATLAB unit-op model is valuable for use between different CAPE-OPEN compliant PMEs.

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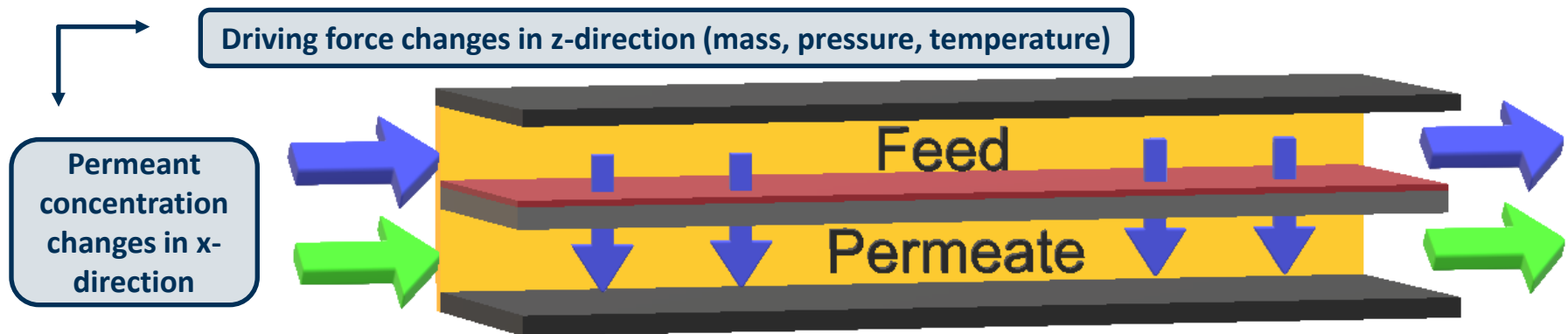
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Future work:

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- Release our CAPE-OPEN unit-op (standalone MATLAB implementation available, [please contact for .zip download](#))

RAPID Center for Process Modeling

Academic Institutions



Dr. Chau-Chyun Chen



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Project Partners



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Thank you for your attention!

Questions?

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Dylan Weber

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Phone: +1.864.202.2298



Supplemental Slides

Our Specific Application

Separation 1 via PIM-1 at a transmembrane pressure of 30 bar

Permeate flux (L/m²/h) 6.33 ± 3.96

=

	Feed Conc.	Permeate Conc.	Permeate Conc.
	mole fraction	mole fraction	Error %
Toluene	0.257	0.267	0.37
Heptane	0.216	0.210	0.95
<i>p</i> -xylene	0.205	0.212	0.47
<i>o</i> -xylene	0.264	0.269	0.74
<i>iso</i> -cetane	0.058	0.042	4.8

Our Specific Application

Separation 2 via SBAD-1 at a transmembrane pressure of 40 bar

Permeate flux (L/m²/h) 0.88 ± 0.52

=

	Feed Conc.	Permeate Conc.	Permeate Conc. Error
	mole fraction	mole fraction	%
Toluene	0.171	0.201	1.5
methylcyclohexane	0.281	0.253	0.79
1-methylnaphthalene	0.020	0.028	3.6
Decalin	0.107	0.110	0.91
<i>n</i> -octane	0.221	0.245	2.0
<i>iso</i> -octane	0.150	0.123	6.5
tert-butylbenzene	0.022	0.027	3.7
1,3,5- triisopropylbenzene	0.016	8.2×10^{-3}	12
<i>iso</i> -cetane	0.013	4.5×10^{-3}	22

Our Specific Application

Separation 3 via SBAD-1 at a transmembrane pressure of 30 bar

Permeate flux (L/m²/h) 0.40 ± 0.12

=

	Feed Conc. mole fraction	Permeate Conc. mole fraction	Permeate Conc. Error %
Toluene	0.284	0.318	1.9
<i>iso</i> -octane	0.388	0.422	1.4
<i>iso</i> -cetane	0.328	0.260	4.2

Ideal Solution vs. Real Mixture Predictions

Comparing ideal solution (IS) and real mixture (RM) predictions for the most complex 9 component permeation simulation:

RM	Full MS, no diff coupling, Vignes avg FH-LM	
	Molar Comp	Partial Flux (LMH)
	0.1995	0.1708
	0.3158	0.3252
	0.0239	0.0269
	0.0789	0.0995
	0.2469	0.3243
	0.0977	0.1299
	0.0227	0.0284
	0.0103	0.0198
	0.0043	0.0102
	1.1350	Total Flux (LMH)

TOL
MCH
MNP
DEC
NOC
IOC
TBB
TIPB
ICE

IS	Full MS, no diff coupling, Vignes avg FH-LM	
	Molar Comp	Partial Flux (LMH)
	0.2002	0.1700
	0.3136	0.3203
	0.0242	0.0270
	0.0804	0.1006
	0.2457	0.3201
	0.0995	0.1313
	0.0231	0.0287
	0.0099	0.0190
	0.0033	0.0078
	1.1249	Total Flux (LMH)

All mixture composition and total flux predictions get marginally better (~3%)

Ideal Solution vs. Real Mixture Predictions

After looking into the details, the feed and permeate activity coefficients are almost identical and this acts to “cancel out” the nonideality on both sides.

Feed-side (phase I) activity coefficients

1.4445
1.0969
2.1656
1.0138
0.9678
1.1228
1.0836
0.9311
0.7949

Permeate-side (phase III) activity coefficients

TOL	1.4413
MCH	1.1111
MNP	2.0411
DEC	0.991
NOC	0.969
IOC	1.1317
TBB	1.051
TIPB	0.9001
ICE	0.7895

After arbitrarily setting the activity coefficients for phase III to be different, IS vs RM predictions were vastly different (50-100%). Generally, the use of real mixture predictions is needed.

Process Flowsheet Modeling and Membrane Unit-Ops

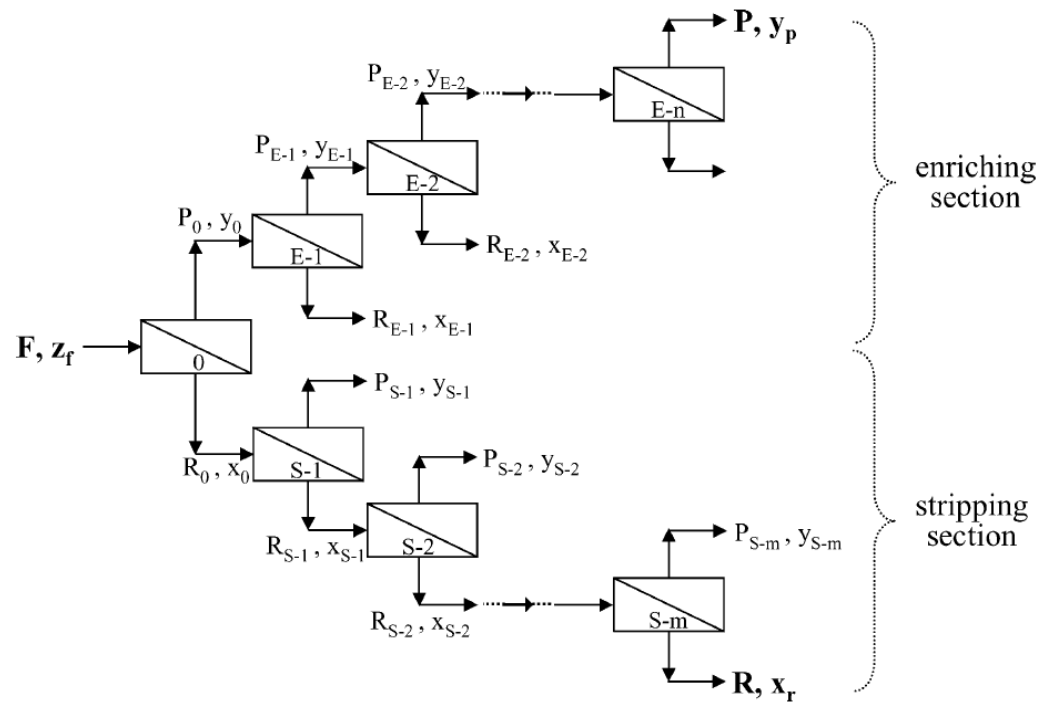
The advantages of including industrial membrane unit operation models within overall process flowsheet simulations include⁷:

7. Kancherla, R., Nazia, S., Kalyani, S., and Sridhar, S. (2021). Modeling and simulation for design and analysis of membrane-based separation processes. Computers Chemical Engineering, 148:107258.

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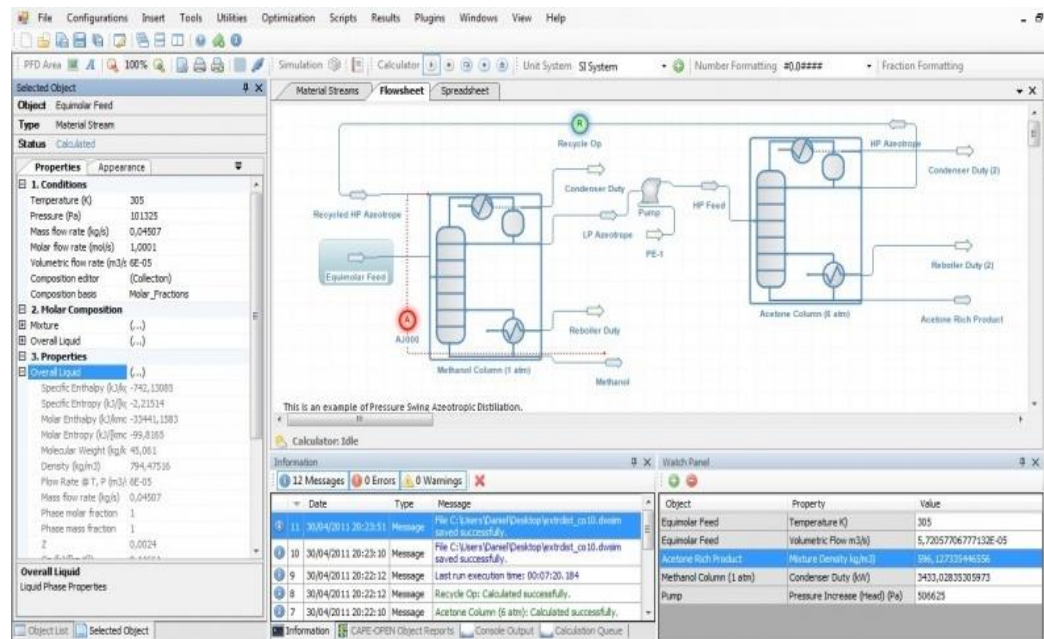
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- Predict process sustainability and techno-economic (TEA) competitiveness versus energy intensive separation methods

Process Flowsheet Modeling and Membrane Unit-Ops

Realistically, this work will be a step forward towards widespread industrial adoption of membrane processes involving complex mixtures

